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<p>(21) International Application Number: PCT/US89/03009 (22) International Filing Date: 11 July 1989 (11.07.89) (30) Priority data: 219,990 14 July 1988 (14.07.88) US</p> <p>(71) Applicant: BOMED MEDICAL MANUFACTURING, LTD. [US/US]; 5 Musick, Irvine, CA 92718 (US). (72) Inventor: Sramek, Bohumir ; 19211 Edgehill Drive, Irvine, CA 92715 (US). (74) Agents: SIMPSON, Andrew, H. et al.; Knobbe, Martens, Olson and Bear, 620 Newport Center Drive, 16th Floor, Newport Beach, CA 92660 (US).</p>		(81) Designated States: AT (European patent), BE (European patent), CH (European patent), DE (European patent), FR (European patent), GB (European patent), IT (European patent), JP, LU (European patent), NL (European patent), SE (European patent). Published <i>With international search report.</i>
<p>(54) Title: MANAGEMENT OF HEMODYNAMIC STATE OF A PATIENT</p> <p>(57) Abstract</p> <p>A therapeutic system provides a clinician with an appropriate course of treatment for a patient whose cardiovascular system is operating outside the normal range of values for the left cardiac work index (LCWI) and the systemic vascular resistance index (SVRI). The left cardiac work index and the systemic vascular resistance index are calculated from the cardiac index (CI) and mean arterial blood pressure (MAP) and are displayed as relative values so that the clinician can readily determine which of the vascular parameters are outside the normal range. Preferably, the cardiac index and the other cardiac parameters are measured by an electrical bioimpedance monitor (104) that provides continuous dynamic measurement of the parameters. The left cardiac work index and the systemic vascular resistance index are calculated by a personal computer (140) that displays the calculated parameters in an easily discernible manner.</p>		

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MANAGEMENT OF HEMODYNAMIC STATE OF A PATIENT

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Background of the Invention

The present invention relates to a method and
apparatus for the non-invasive diagnosis and therapeutic
management of patients having systemic hypertension or
15 other critical illnesses, and, more particularly, to a
method and apparatus for determining a therapy to achieve
both a normotensive and normodynamic state or a selected
state dictated by conditions to increase the probability
of survival after surgery, trauma, illness, or the like.

20 Hypertension is typically diagnosed through a non-
invasive measurement of systolic and diastolic arterial
pressure values by a sphygmomanometer, and by comparing the
obtained "blood pressure" values to values considered
"normal" for that particular patient taking into
25 consideration the sex, age and body habitus. Once
diagnosed, hypertension today is predominantly treated by
prescription of any of a variety of classes of drugs which
are pharmacologically capable of reducing the measured
blood pressure value. Hypertension is then considered
30 under control when the measured arterial pressures reach
the normal range.

Although the use of such single modality therapy is
generally quite successful in achieving the desired
variation in the measured blood pressure, it does not take
35 into account the patient's status with regard to more
important hemodynamic parameters, such as cardiac output.
Hypertensive drugs can be prescribed which have the

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additional and unmeasured effect of simultaneously lowering cardiac output. Thus, notwithstanding attainment of the normotensive end goal of therapy, important hemodynamic deviations can remain, or even be induced by the prescribed 5 therapy. The resulting diminished perfusion could be reasons for so-called side effects of hypertension therapy, such as dizziness, impotence and general down feeling, which the patient typically did not experience prior to diagnosis and traditional treatment of hypertension.

10 Hence, current hypertension therapy could lead to prolonged duration of the treatment, higher cost to the patient and/or medical insurance carrier, adverse side effects resulting in patient's noncompliance, and general lowering of the patient's quality of life.

15 The importance of precise differentiation between normotensive therapy and effects on the hemodynamic state have recently been underscored by the work of W.C. Shoemaker, M.D., Department of Surgery, UCLA Medical Center, in the postoperative critically ill patient. While 20 studying postoperative, high-risk, critically ill survivors and non-survivors, Shoemaker found that, in general, the survivors' cardiovascular systems maintained mean arterial pressure at a normotensive level while increasing their global blood flow to a cardiac index of greater than 4.5 liters/min/m² and maintaining it at that level throughout 25 the postoperative period.

In contrast, the non-survivors did not experience increased global blood flow during the postoperative period. The non-survivors generally were normotensive and 30 maintained blood flow at a cardiac index of 3.5 liters/min/m² which is considered normal for healthy adults.

The surgical wound requires significantly increased perfusion to facilitate healing and the removal of fluids. 35 Thus, in order to maintain adequate perfusion of all organs, the global blood flow must increase. If this condition is not met, the brain will reduce flow to

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selected organs in order to maintain increased perfusion of the surgical site. The organs inadequately perfused will eventually fail. Shoemaker found that the mean time at which the deaths of non-survivors occurred was approximately 90 hours postoperatively as a result of single or multiple organ failure.

Subsequently, in a controlled study, Shoemaker proved that in patients who are not in hyperdynamic sepsis and whose cardiovascular systems cannot increase the level of global blood flow to a desired hyperdynamic level, proper immediate postoperative management through volume expansion, positive inotropic support and peripherally vasoactive therapy, resulting in a cardiac index greater than 4.5 liters/min/m² and normotension (mean arterial blood pressure approximately equal to 92 Torr), will substantially increase their chances to survive.

The implementation of the foregoing therapeutic goal has the potential for a dramatic reduction of postoperative mortalities, estimated to be approximately 400,000 annually in the U.S. alone.

Summary of the Invention

There has been provided in accordance with one aspect of the present invention a method of achieving a preselected hemodynamic state in a subject mammal, typically a human patient. The preselected hemodynamic state may be a state of normovolemia, normoinotropy and arterial normocapacitance, although the preselected state may be another hemodynamic state, if indicated by the circumstances surrounding diagnosis and treatment. The method comprises the steps of first determining the mean arterial pressure of the patient and then measuring the cardiac index of that patient. Left cardiac work index (LCWI) is determined based upon the foregoing measured values, in accordance with the formula:

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wherein MAP represents mean arterial pressure, PAOP represents pulmonary artery occluded pressure, CI represents cardiac index and K is a constant. Typically, PAOP may be assumed to be approximately 6 Torr. The 5 patient's systemic vascular resistance index (SVRI) is additionally determined utilizing the measured values of mean arterial pressure and cardiac index, according to the formula:

10
$$\text{SVRI} = \frac{(\text{MAP} - \text{CVP}) \times 80}{\text{CI}}$$

wherein CVP is central venous pressure, which typically may be assumed to be approximately 3 Torr. The obtained LCWI and SVRI values are thereafter compared to the values 15 desired to be obtained in the patient, and a therapeutic dose of a pharmacologically active material is administered for altering these values to achieve the preselected hemodynamic state. In a case where the preselected hemodynamic state in an adult patient comprises arterial 20 normocapacitance, the pharmacologically active material comprises a vasodilator if the systemic vascular resistance index exceeds about 2030 dyn·sec/cm^{5m²}. Alternatively, if the systemic vascular resistance index is less than about 2030 dyn·sec/cm^{5m²}, the pharmacologically active material 25 comprises a vasoconstrictor.

In a case in which the end goal of therapy is achieving normovolemia and normoinotropy, the pharmacologically active material comprises one which will have a volume expansion and/or positive inotropic effect if the left cardiac work 30 index is less than about 4.35 kg·m/m². Alternatively, volume reduction and/or negative inotropic therapy will be indicated in a patient having a left cardiac work index in excess of about 4.35 kg·m/m².

Further features and advantages of the present 35 invention will become apparent from the Detailed Description of Preferred Embodiments which follows, when considered together with the attached figures.

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Brief Description of the Drawings

Figure 1 illustrates the interrelationship between cardiac index, mean arterial pressure, systemic vascular resistance index and left cardiac work index in a human adult.

Figure 2 illustrates the interrelationship between cardiac index, mean arterial pressure, systemic vascular resistance index and left cardiac work index in a human adult showing the changes in the parameters caused by triple modal therapy (e.g., volume reduction/negative inotropic/ vasodilation).

Figure 3 illustrates the interrelationship between cardiac index, mean arterial pressure, systemic vascular resistance index and left cardiac work index in a human adult showing the changes in the parameters caused by triple modal therapy including the stronger utilization of negative inotropes in conjunction with lowering the heart rate, supplemented by volume reduction.

Figure 4 illustrates a schematic representation of an electronic system to assist in providing the diagnostic and therapeutic information in accordance with the method of the present invention.

Figure 5 illustrates an exemplary data format for the serial output transmitted from the exemplary NCCOM®3-R7 electrical bioimpedance monitor to the computer in Figure 4.

Figure 6 illustrates an exemplary system of the present invention that includes an automatic pressure measuring system.

Figure 7 illustrates an exemplary system of the present invention that includes an alternative automatic pressure measuring system that utilizes electrical bioimpedance techniques.

Figure 8 is a flow chart of an exemplary computer program algorithm for implementing the present invention.

Figure 9 illustrates an exemplary screen display that utilizes bar graphs to display the parameters of the

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hemodynamic status of a patient's cardiovascular system for use in diagnostic evaluation of a patient.

Figure 10 illustrates an alternative screen display that utilizes cartesian graphs to display the hemodynamic 5 status and the percentage deviation from a selected goal of a patient's cardiovascular system.

Figure 11 illustrates the cartesian graph screen display of Figure 10 for a patient having 43% relative 10 hypovolemia and/or hypoinotropy and arterial normocapacitance.

Figure 12 illustrates the cartesian graph screen display of Figure 11 for the same patient and the same input parameters but with the coordinates of the graph adjusted for a therapeutic goal of increased oxygen 15 perfusion, showing that, for this therapeutic goal, the patient has an increased percentage of relative hypovolemia and/or hypoinotropy and has relative arterial hypocapacitance.

Detailed Description of Preferred Embodiments

20 The primary function of the cardiovascular system is transport of oxygen. Pulsatile pressure having a mean component (mean arterial pressure or MAP) develops as a byproduct of the viscosity of blood pushed out of the left ventricle and through the vasculature system which is characterized by a systemic vascular resistance (SVR). The 25 systemic vascular resistance and mean arterial pressure are related such that in the absence of corrective mechanisms, a reduction in SVR through vasodilatation will result in a reduction in pressure. However, it is generally recognized that the supply of oxygen to all tissue cells is a function 30 of global blood flow, i.e., cardiac output, and not blood pressure as will become apparent.

Determination of MAP is typically achieved using a sphygmomanometer to directly determine systolic and 35 diastolic pressure, and solving the following equation:

$$\text{MAP} = \frac{\text{SYSTOLIC} - \text{DIASTOLIC}}{3} + \text{DIASTOLIC} \quad (1)$$

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MAP values may also be measured and displayed directly on automated blood pressure instruments using oscillometric principles.

There currently exist about eight practical methods of measuring cardiac output, including three indicator dilution methods (known as FICK, dye and thermodilution), three methods which allow visualization of heart chambers and a subsequent calculation of stroke volume and cardiac output (cine-angiography, gated pool radionuclides, echocardiography) and two other methods (Doppler ultrasound and electrical bioimpedance). The only absolutely accurate blood flow measurement method, not mentioned above, is a calibrated cylinder to collect blood and a stopwatch. Of course, each of the foregoing methods is characterized by a unique balance of accuracy, invasive/non-invasive nature, and patient risk, as will be appreciated by one of skill in the art.

Although any of the foregoing known methods of determining cardiac output may be used, the mechanics of each being well known in the art, it is preferred in the context of the present invention to non-invasively and continuously monitor cardiac output through the use of an instrument such as the NCCOM®3-R7 manufactured by BoMed® Medical Manufacturing Ltd. in Irvine, California, which is the subject matter of U.S. Patent No. 4,450,527, which is incorporated herein by reference. This instrument has been determined to exhibit the same accuracy as any of the available alternative methods, while accruing the substantial advantage of being a non-invasive technique.

In addition to determining cardiac output, several additional parameters can be measured noninvasively utilizing the NCCOM®3-R7, as a result of its use of Thoracic Electrical Bioimpedance (TEB) technology. TEB measures total electrical impedance of the thorax which is called TFI (Thoracic Fluid Index) and which is volume dependent. TFI has a normal range in males between 20 and 33 Ohms and in females between 27 and 48 Ohms. A lower TFI

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value indicates an excess of fluids (more conductive thorax).

TEB also measures two parameters which are related to measurement of contractility. Index of Contractility, 5 (IC), is a volume-dependent measure of the contractile state and ACI (Acceleration Index) is a volume-independent measure of the inotropic state. The normal range for IC in a human adult falls between about 0.033 to about 0.065/sec, and the normal range for ACI is between about 0.5 and about 10 1.5/sec². TEB measurements may conveniently be performed using the BoMed NCCOM[®]3-R7, and provide useful supporting data as will be discussed.

Once MAP and CI are known, two additional important hemodynamic parameters can be determined. The first is the 15 systemic vascular resistance index (SVRI) defined by the arithmetic ratio of the arterial-venous pressure difference and an indexed blood flow in accordance with the following equation:

$$20 \quad SVRI = \frac{(MAP - CVP) \times 80}{CI} \quad (2)$$

In this equation, CVP is central venous pressure measured in Torr, 80 is a constant of proportionality and CI is the cardiac index. Since the value of cardiac output (CO) is a 25 direct function of body mass, its normalized value, e.g., cardiac index (CI) is a more appropriate indicium for assessing adequacy of perfusion. Similarly, with systemic vascular resistance being flow dependent and, therefore, body size-dependent, its direct use is unhelpful for 30 absolute quantification of the normal levels of arterial capacitance. Thus, its indexed value, SVRI, will be discussed herein. If cardiac index (CI) is used as in Equation (2), the equation will directly provide the indexed parameter SVRI. The NCCOM[®]3-R7, for example, 35 allows a clinician to enter either the patient's body weight or the patient's body surface area to provide a basis for calculating the indexed outputs.

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The data obtained through Equation (2) will not be subject to a significant error if CVP = 3 Torr is assumed to be a typical value in the usual patient. In some cases, of course, the CVP can vary from as low as about 0 (zero) 5 Torr to as high as about 10 Torr under different hemodynamic conditions. Minor variations from 3 Torr are generally insignificant since CVP is subtracted from the much larger MAP which may range from approximately 93 Torr in the normotensive patient to as high as 120 Torr as in Example 2 10 (described hereinafter), or higher in a hypertensive patient.

A second important hemodynamic parameter that can be calculated once MAP and CI are known, is the left cardiac work index (LCWI) defined by the arithmetic product of the 15 pump's pressure contribution and blood flow as expressed in the following equation:

$$LCWI = (MAP - PAOP) \times CI \times 0.0144 \text{ kg} \cdot \text{m/m}^2 \quad (3)$$

wherein PAOP is pulmonary artery occluded pressure in Torr, CI is cardiac index in liters/min/m², and 0.0144 is a constant of proportionality. In the typical patient, the PAOP will be approximately 6 Torr, and this value may be ordinarily assumed without subjecting the data to any significant error. However, a patient's actual PAOP can vary sufficiently to justify determination of the actual 25 PAOP value for use in Equation (3) under conditions of pump failure. In such a case, the actual PAOP can be determined invasively using a thermodilution catheter.

Depending upon oxygen demand, the heart has a capability to vary cardiac output by a factor of 10, all 30 within the life-sustaining range, throughout which MAP is maintained by the brain at a fairly constant level due to several biofeedback mechanisms with different time constants. Thus, the brain continually re-evaluates Equation (2) to maintain MAP constant, and a decrease in 35 SVRI (increase in global oxygen demand) must be met by an equal percentage increase of CI (increase in oxygen

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delivery) in order to maintain MAP constant. Thus, the brain attempts to maintain MAP constant by simultaneously varying SVRI by vasoactivity and output of the pump by heart rate, preload, contractility and afterload.

5 Essential hypertension, as generally understood today, is probably caused by a gradual increase of stiffness of arterial walls which results in an increase in vascular impedance, or by a gradual decrease of vascular capacitance, e.g., gradual vasoconstriction. Both cases
10 result in an increase of SVRI. In order to provide adequate perfusion, (which, for an adult is approximately 3.5 liters/min/m²), under conditions of an elevated SVRI, the brain must permit a rise in MAP to accommodate Equation
15 (2). This is a hemodynamic explanation of essential hypertension.

Since, in the case of essential hypertension, the body must increase MAP in order to provide adequate perfusion, the worst choice of therapy would be to prescribe drugs to lower MAP (which the clinician can easily measure) and,
20 unfortunately also simultaneously lower CI (which the clinician typically does not measure). The resulting diminished perfusion could be reasons for the so-called side effects of hypertension therapy including dizziness, impotence and general down feeling, which the patient often
25 did not experience prior to institution of the hypertension therapy.

The end goal of essential hypertension therapy should therefore be to lower the blood pressure to an acceptable, e.g., normotensive level, while maintaining adequate perfusion. This cannot be accomplished by measuring mean arterial pressure alone, but must also involve the determination of the deviation, if any, from arterial normocapacitance and normovolemia and/or normoinotropy, based upon measured values for MAP and cardiac index.
35

35 The mutual interrelationships between MAP, CI, LCWI and SVRI for the supine resting adult, defined by Equations (2) and (3) above, are illustrated in Figure 1. Since MAP

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and CI can be directly measured, they become coordinates of the orthogonal system while LCWI and SVRI become the derived parameters. From this chart, the approximate values of LCWI and SVRI can be visually observed without 5 the necessity of going through the foregoing equations.

The range of normal MAP, illustrated in Figure 1 at numeral 10, and the range of normal CI 12 define two main perpendicular axes of an ellipse 14 encompassing the loci of all normotensive and normodynamic patients. The center 10 16 of the ellipse 14 represents an ideal mean-mean value and could be considered an appropriate end goal of therapy for patients whose data describes a point outside of the normal ranges. Since the ideal MAP and CI are described in terms of ranges, however, and not absolute values, the data 15 derived from a normotensive and normodynamic patient will define a point on Figure 1 which may be anywhere within ellipse 14. Ellipse 14 reflects the empirically derived data that MAP_{mean} equals 92 Torr, with a range of normotension from about 84 to about 100 Torr depending on 20 the hemodynamic state. In addition, the CI_{mean} equals 3.5 liters/min/m², with a normodynamic range of from about 2.8 to about 4.2 liters/min/m² in the resting human adult depending upon the hemotensive state.

The LCWI lines 18 run from the upper left of Figure 1 25 to the lower right. The particular LCWI lines (not illustrated) which are tangent to the ellipse 14 define the bounds of the normal range of LCWI for adult humans. The SVRI lines 20 run from the upper right of Figure 1 to the lower left. Similarly, the particular SVRI lines (not 30 illustrated) which are tangent to the ellipse 14 (not illustrated) define the bounds of the normal range of SVRI for human adults. Although literature-published data of normal ranges of LCWI and SVRI, based on demographic data collected by any particular author, can vary considerably, 35 the following are believed representative of a significantly large population and have, therefore, been incorporated into Figure 1: $LCWI_{mean} = 4.35 \text{ kg}\cdot\text{m}/\text{m}^2$;

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normal LCWI range is between about 3.3 and 5.3 kg·m/m²; SVRI_{mean} = 2030 dyn·sec/cm⁵m²; and the normal SVRI range is between about 1660 and 2580 dyn·sec/cm⁵m². For neonatal patients, the normal LCWI range is between about 2.5 and 5 4.0 kg·m/m², and the normal SVRI range is between about 950 and 1500 dyn·sec/cm⁵m².

The loci of constant LCWI (the hyperbola 18) simultaneously represent the isovolemic and/or isoinotropic lines. Hence, the LCWI line passing through the center of 10 the ellipse 14 (LCWI = 4.35 kg·m/m²) is the line of normovolemia and/or normoinotropy. A patient who is in the center of the normotensive and the normodynamic ranges is also normovolemic and normoinotropic.

The foregoing results from the fact that the heart is 15 neither a constant volume nor a constant pressure pump. By circulating non-compressible fluid through the system which exhibits a given value of SVRI, it creates MAP with a certain level of arterial distention. For example, consider a patient exhibiting a starting state. 20 corresponding to point 16 on Figure 1 wherein CI = 3.5 liters/min/m², MAP = 92 Torr, and SVRI = 2030 dyn·sec/cm⁵m². If the system would vasoconstrict to SVRI = 2440 dyn·sec/cm⁵m², MAP would increase in an attempt 25 to maintain an adequate level of perfusion. If the circulation level would remain the same (CI = 3.5 liters/min/m²), MAP would increase to 110 Torr (point 22 on Figure 1), causing additional arterial distention through an increase in intravascular pressure, hence an increase of volume. On the other hand, if the 30 system would maintain the same volume while vasoconstricting to SVRI = 2440 dyn·sec/cm⁵m² level, it would reach MAP = 101 Torr (point 24 on Figure 1) but would have to simultaneously decrease CI to 3.2 liters/min/m². LCWI = 4.35 kg·m/m² is, therefore, a line of a constant volume.

35 Patients having an LCWI value lower than about 4.35 kg·m/m² are either hypovolemic or hypoinotropic, or a combination of both. Conversely, if the patient's LCWI

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value is higher than about $4.35 \text{ kg} \cdot \text{m}^2$, the patient's heart is not only burning a greater amount of oxygen but the patient is also hypervolemic or hyperinotropic, or a combination of both. The volemic and inotropic status of a 5 patient are masked by each other on Figure 1 when considering the patient's MAP and CI alone. However, whether a deviation in LCWI is due to an abnormal volemic or inotropic state can be differentiated through consideration of the supporting TEB data, as illustrated in 10 Example 1.

The LCWI hyperbolas 18 are marked in Figure 1 both by their respective $\text{kg} \cdot \text{m}^2$ value and by the percentage deviation from normovolemia and/or normoinotropy. The negative deviations represent hypovolemia and/or 15 hypoinotropy, whereas the positive deviations represent hypervolemia and/or hyperinotropy. Figure 1 illustrates 20% increments in deviations of hyper/ hypovolemia and/or hyper/hypoinotropy, since the volemic and inotropic deviation is more important in diagnostic and therapeutic 20 decision-making than the abstract LCWI value.

The foregoing ellipse 14 in Figure 1 is based upon the data obtained from normal adult patients. A similar ellipse 19 can be constructed for neonatal infants based upon a range of $\text{CI} = 4.2 \pm 20\% \text{ liters/min/m}^2$ and a range of 25 $\text{MAP} = 60 \pm 10\% \text{ Torr}$. A line (not shown) connecting the centers of the ellipse 14 for adults and the ellipse 19 for neonates would reflect the effects of aging on hemodynamic parameters. Any of a number of additional ellipses could be constructed for any age group. For example, an ellipse 30 (not shown) defining the empirically observed normotensive and normodynamic ranges in premature infants would be below and slightly to the right from the neonate ellipse. Ellipses for pediatric patients, depending upon their age, would appear between the ellipse 14 for adults and the 35 ellipse 19 for neonates.

The SVRI line 20 passing through a specific patient's point (located at the intersection of his/her MAP and CI

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values) represents the direction of the highest gradient of the hemodynamic response to fluid expansion/reduction and/or to inotropic therapy and provides the vectorial direction of that specific therapy. For example, volume 5 expansion and/or positive inotropic therapy will move the patient's point along the SVRI line toward upper right in Figure 1, whereas volume reduction and/or negative inotropic therapy will move the patient's point toward the lower left of the chart in Figure 1.

10 The SVRI lines 20 on Figure 1 also represent the arterial isocapacitance lines. Arterial capacitance is a physical description of the state of vasoactivity: hypcapacitance represents a vasoconstricted arterial bed, whereas hypercapacitance represents a vasodilated arterial 15 bed. The SVRI line 20 passing through the center 16 of the normotensive/normodynamic ellipse 14 drawn on Figure 1 (SVRI = 2030 dyn.sec/cm^{5m²}) represents the line of arterial normocapacitance. (A normotensive and normodynamic patient also exhibits arterial normocapacitance.) The LCWI line 18 20 passing through a specific patient's point represents the highest gradient of change of vasoactivity, hence the vectorial direction of the peripheral vasoactivity therapy.

The SVRI values higher than about 2030 dyn.sec/cm^{5m²} correspond to states of arterial hypcapacitance. Such 25 patients will require peripheral vasodilatation therapy to rectify their arterial capacitance deviation. The SVRI values lower than the arterial normocapacitance line value represent arterial hypercapacitances. The patients with these values of SVRI will require peripheral 30 vasoconstriction to render them arterially normocapacitive. Again, the negative deviations of SVRI represent arterial hypcapacitances (vasoconstricted system), the positive deviations represent arterial hypercapacitances (vasodilated system).

35 From the discussion above, it is clear that volume expansion and positive inotropic therapy both have the same vectorial effect (up and to the right along the patient's

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SVRI line). Similarly, the volume reduction and negative inotropic therapies mask each other with the same vectorial effect (down and to the left along the patient's SVRI line). If a mean normotensive and normodynamic state (the center 16 of the ellipse 14) is the therapeutic goal, the use of volume expansion or volume reduction therapy as a single modality therapy is only appropriate on patients who happen to exhibit arterial normocapacitance ($SVRI = 2030 \text{ dyn} \cdot \text{sec}/\text{cm}^5\text{m}^2$) and whose only hemodynamic abnormality is a deviation from normovolemia. A similar statement is valid for a supplemental inotropic therapy, which can be used to augment inadequate hemodynamic response to volume expansion/reduction.

Similarly, the use of a single modality peripherally vasoactive therapy can only be appropriate for a patient whose hemodynamic points happen to fall along the normovolemic and/or normoinotropic line ($LCWI = 4.35 \text{ kg} \cdot \text{m}/\text{m}^2$).

However, considering statistical distribution of an infinite number of MAP and CI pairs, a vast majority of patient points will fall outside of these two specific lines related to a single modality therapy. These patients will require a complex, multi-component volemic and cardioactive drug therapy. In accordance with the invention disclosed herein, it becomes clear that the first goal of such therapy should be to correct any fluid deficiency or excess, and the second goal should be to choose proper drug therapy which will institute a normal (or selected) hemodynamic condition.

For these patients in whom single modality therapy is inappropriate, therapy should be initiated which will give rise to vectorial components on Figure 1 parallel with each set of SVRI and LCWI lines, such that when vectorially added, will render the patient normotensive and normodynamic. Thus, the correct therapy will result in a vectorial sum of effects of volume expansion and/or reduction, together with positive and/or negative inotropic

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therapy and a vectorial sum of vasodilatation and/or vasoconstriction that will move the patient's point to within the ellipse 14. The specific percentage deviation from the ideal goal of therapy which can be derived from 5 Figure 1 will assist the clinician to quantify the titration of that specific therapeutic component.

The following two examples illustrate the efficacy of utilizing the method of the present invention in one common class of hemodynamic deviation which could benefit from 10 correct non-invasive assessment -- the treatment of essential hypertension. The examples involve two patients who were both undergoing treatment for hypertension for over one year but remained hypertensive and were both at approximately the same level of MAP though each in a 15 different cardiodynamic state. Thus, they each required a completely different choice of therapy.

EXAMPLE 1

Male patient, 61 years old, height 173 cm, weight 78 kg, was first diagnosed hypertensive 13 years ago. He 20 had been taking orally, once a day for the last three months, INDERIDE LA 80/50 mg (a long-acting combination of beta blockers and diuretics). The INDERIDE replaced the previous therapy which involved the use of diuretics for many years. The main reason for the change in prescription 25 was the side effects of the simple diuretic therapy, such as cold extremities, which improved after switching to INDERIDE. The INDERIDE therapy lowered MAP into the 110 Torr level from the MAP = 133 Torr level (190/105 Torr) which the patient would attain without medication. The 30 therapy never lowered the value of his arterial pressure below MAP = 110 Torr. The patient's hemodynamic and cardiodynamic state was measured with Bomed's NCCOM[®] 3-R7 and a sphygmomanometer. This state is shown at the point identified by reference numeral 26 in Figure 2, which 35 corresponds to a MAP of 110 Torr (hypertensive) and a CI of 2.6 liters/min/m² (hypodynamic). The supporting TEB

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measurements were TFI = 29.8 ohm, IC = 0.038/sec, ACI = 1.05/sec², and HR = 58 beat/min.

The physiologic interpretation of point 26 derived from Figure 2 is relative hypovolemia and/or relative 5 hypoinotropy 10%, relative arterial hypocapacitance 60%. The TEB data above confirm normal inotropic state (a normal ACI value) pointing to relative hypovolemia as the contributor to the 10% deviation. However, the major 60% physiologic deviation is excessive vasoconstriction for 10 which this patient has not been treated at all.

After the data analysis, the patient was administered 50 mg of CAPOTEN (peripheral vasodilator), and a new measurement of his hemodynamic parameters was performed six hours later (estimated half-time of CAPOTEN). This new 15 measurement is expressed as a movement of his hemodynamic state from the initial state -- point 26 to point 28 in Figure 2. The new data relating to the patient's condition following administration of CAPOTEN are:

MAP.	92 Torr (mean normotensive)
20 CI	3.4 liters/min/m ² (normodynamic)
TFI	28.4 ohm
IC	0.043/sec
ACI	1.18/sec ²
HR	69 beats/min.

25 The patient is now both normotensive and normodynamic, and has been maintained in this state by staying on the original prescription of INDERIDE LA 80/50 once a day supplemented by CAPOTEN 50 mg taken twice daily. This triple modality therapy (volume reduction/negative 30 inotropic/ vasodilatation) is, according to analysis of the statistical distribution of patient points on Figure 1, the most often required therapy for treatment of hypertension, though currently seldom practiced. Potential fine-tuning of the therapy in this patient could require a reduction of 35 titration of diuretics to 25 mg/day.

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EXAMPLE 2

Female patient, 44 years old, height 153 cm, weight 47 kg, treated for severe hypertension for 12 months. Most recently, she has been taking CALAN SR 240 mg (calcium channel blocker) and HYDROCHLOROTHIAZIDE 25 mg (diuretic) daily. The therapy never reduced her MAP below 110 Torr. She also complained about several side effects.

The patient's hemodynamic state was measured with the same instrumentation as in Case 1. Her hemodynamic state 10 is expressed as point 30 in Figure 3:

	MAP	120 Torr
	CI	4.9 liters/min/m ²
	TFI	24.4 ohm
	IC	0.081/sec
15	ACI	2.28/sec ²
	HR	73 beats/min

The position of point 30 in Figure 3 shows a 15% deviation toward arterial hypercapitance and 90% toward hypervolemia and/or hyperinotropy. The supporting TEB data 20 above document that (a) the patient is hyperdynamic (CI and SI values much higher than their normal range), (b) hypervolemic (TFI value is significantly below normal range for females indicating an excess of fluids), and (c) hyperinotropic (ACI and IC values higher than their normal 25 range). The 90% increase of LCWI also demonstrates a potential long-term problem of the patient's condition -- excessive work of the pump (excessive myocardial consumption). In the absence of the knowledge that the patient is hyperdynamic, she could never have been treated 30 correctly.

Analysis of the data corresponding to point 30 on Figure 3 clearly points toward a therapy which should include (a) stronger utilization of negative inotropes in conjunction with (b) lowering heart rate, supplemented by 35 (c) volume reduction.

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The patient was administered INDERIDE LA 80/50 mg. The patient's parameters were then measured again after 24 hours. The new hemodynamic data are expressed as movement of the patient's hemodynamic point from the point 30 to 5 point 32 in Figure 3. The patient's data corresponding to point 32 were:

	MAP	93 Torr (normotension)
	CI	4.1 liters/min/m ²
	TFI	28.6 ohm (now within normal range)
10	IC	0.071/sec
	ACI	1.86/sec ²
	HR:	58 beats/min

The patient began taking INDERIDE LA 80/50 mg once a day and was maintained normotensive and normodynamic. 15 However, during twice-daily blood pressure measurements, it was noted that 12 hours after taking the drug, her MAP decreased to a value of MAP = 90 Torr, while 24 hours later (at the time of taking another dose), it was consistently at a value of MAP = 98 Torr. She was metabolizing the drug 20 at a faster rate, causing larger periodic variation of the drug level in her system. To prevent such a hemodynamic variation, the prescription was split and skewed by 12 hours. INDERAL LA 80 mg is now taken once a day and the diuretic (50 mg) taken also once a day, though 12 hours 25 later. The patient's MAP is maintained this way at 93 Torr level, and the patient is hemodynamically stable without the side effects reported on the initiation of this study.

The preceding case studies illustrate the proper measurement and identification of a patient's hemodynamic 30 and physiologic state in accordance with the method of the present invention. This can be easily accomplished and the deviation from the ideal state clearly defined. The patient can be treated so as to achieve an ideal (or selected) hemodynamic state in real time. Significantly, 35 the important results of the described method are obtainable

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based upon non-invasive physiologic and hemodynamic measurements.

Description of An Exemplary Electronic System for Implementing the Method of the Present Invention

5 Figure 4 is a schematic representation of an exemplary electronic system for implementing the method of the present invention. As illustrated, a patient 100 is electrically connected to an electrical bioimpedance monitor (EBM) 104, which, preferably, is an NCCOM®3-R7 noninvasive continuous
10 cardiac output monitor manufactured by BoMed Medical Manufacturing Ltd. of Irvine, California. The electrical bioimpedance monitor 104 is connected to the patient 100 via a first electrical conductor 110 connected to a first connector 111, a second electrical conductor 112 connected
15 to a second connector 113, a third electrical conductor 114 connected to a third connector 115, and a fourth electrical conductor 116 connected to a fourth connector 117. The first electrical conductor 110 is connected to a first pair
20 of electrodes 120a and 120b that are positioned on the neck of the patient 100 at the intersection of a line encircling the root of the neck with the frontal plane of the patient 100 (the frontal plane is an imaginary plane dividing the anterior and posterior sections of the neck and shoulder of the patient 100). Thus, the two electrodes 120a and 120b
25 are positioned approximately 180° apart around the circumference of the neck. The second electrical conductor 112 is connected to a second pair of electrodes 122a and 122b that are positioned on the patient's neck approximately 5 centimeters directly above the first pair of electrodes
30 120a and 120b. The third electrical conductor 114 is connected to a third pair of electrodes 124a and 124b that are positioned on the patient's thorax along the mid-axillary line at the xiphoid process level with the electrode 124a positioned approximately 180° apart from the
35 electrode 124b. The fourth electrical conductor 116 is electrically connected to a fourth pair of electrodes 126a and 126b that are positioned on the patient's thorax

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approximately 5 centimeters directly below the third pair of electrodes 124a and 124b. It should be understood that the positioning of the electrodes can be varied to accommodate bandages and other obstructions so long as the 5 electrodes in each pair of electrodes are approximately 180° apart. Other electrode combinations (e.g., band electrodes, and the like) can also be used.

The electrical bioimpedance monitor 104 includes a serial data output connector 130 which is electrically 10 connected via a serial data line 132 to a computer 140, such as an IBM® PC, XT, AT, or the like. Other computers can also be advantageously used. The computer 140 is connected to a keyboard 142 and to a monitor 144 that operate in known conventional manners. Preferably, the 15 computer 140 is also connected to a printer 146. The computer 140 receives serial data from the electrical bioimpedance monitor 104, processes the data and displays the processed data on the monitor and the printer. The details of the data received from the electrical bioimpedance monitor 104 and the processing functions of the computer 140 will be discussed in additional detail 20 below. It should be understood that a parallel data connection can also be used between the electrical bioimpedance monitor 104 and the computer 140 in alternative 25 embodiments of the invention.

The electrical bioimpedance monitor 104 further includes a set of electrical output connectors 150 that provide an ECG compatible output signal thereon. The ECG compatible output signal is connectable to a conventional 30 ECG monitoring device 152 via an ECG cable 154. As will be discussed below, the ECG compatible output signal is selectively representative of the electrical activity of the patient's heart or the electrical bioimpedance measurements.

The electrical bioimpedance monitor 104 preferably 35 further includes an ECG input connector 160 that is connectable to a set of conventional ECG electrodes (not shown) on the patient 100 via a set of ECG input lines 162.

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The electrical bioimpedance monitor 104 operates in a known manner to derive significant cardiac information from the electrical bioimpedance changes that occur during each cardiac cycle. Briefly, the electrical bioimpedance monitor 104 operates by generating a high frequency, substantially constant current that is provided as an output from the connectors 113 and 117 (labeled as CIO to represent the current injection outputs). The constant current is coupled to the patient via the second conductor 112 and the fourth conductor 116 and is injected into the body of the patient 100 between the second pair of electrodes 122a and 122b and the fourth pair of electrodes 126a and 126b so that the current flows through the patient's thorax between the two pairs of electrodes. The constant current causes a voltage to be induced in the patient's thorax that is proportional to the electrical impedance of the thorax. The induced voltage is sensed between the first pair of electrodes 120a and 120b and the third pair of electrodes 126a and 126b. The sensed voltage is conducted to the electrical bioimpedance monitor 104 via the first conductor 110 and the third conductor 114 and is provided as an input to the electrical bioimpedance monitor 104 via the connectors 111 and 115 (labeled as SVI to represent the sensed voltage input). The electrical bioimpedance monitor 104 converts the sensed voltage into a representation of the electrical bioimpedance of the thorax. The electrical bioimpedance as a function of time is referred to as $Z(t)$. The representation of the electrical bioimpedance is available as an output on a connector 162.

The electrical impedance of the thorax depends upon a number of factors, one of which is the quantity of blood in the vasculature system of the thorax which changes throughout each cardiac cycle. The electrical impedance changes caused by the blood in the thorax are time-varying and can be detected by differentiating the detected sensed voltage to provide a representation of the differentiated electrical bioimpedance (i.e., dZ/dt) which includes both

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changes caused by blood flow in the thorax and changes caused by respiration and other more slowly changing factors.

The NCCOM[®]3-R7 processes the differentiated bioimpedance information and provides a processed signal that represents the electrical bioimpedance changes (dZ/dt) caused by blood flow. The processed dZ/dt signal is selectively provided as an output signal from the electrical bioimpedance monitor 104 on a dZ/dt output connector 164 so that the dZ/dt signal can be provided as an input to an oscilloscope (not shown) or other suitable equipment for monitoring the dZ/dt signal.

The electrical bioimpedance monitor 104 can also derive an ECG signal from voltages present on the four input lines 110, 112, 114 and 116. The ECG signal which represents the electrical activity of the patient's heart can also be sensed by the four pairs of electrodes described above. The ECG signals can be separated from the sensed voltage proportional to the electrical bioimpedance since the injected constant current signal is a relatively high frequency (e.g., 50-100 kHz) and the ECG signals generated by the heart have a considerably lower frequency content. Thus, suitable filters can be used to separate the two signals. Alternatively, in the event that a suitable ECG signal cannot be derived from the electrical input signals on the four lines 110, 112, 114 and 116, the ECG input connector 160 can be connected to suitably positioned electrodes (not shown) to obtain an ECG input signal. The ECG signal derived from the four input lines 110, 112, 114, and 116, or the ECG signal derived from a separate ECG signal on the ECG input connector 160 is selectively output as an ECG compatible output signal on the set of ECG output connectors 150 that can be recorded and displayed on the ECG monitoring device 152. The preferred embodiment of the electrical bioimpedance monitor 104 (e.g., the NCCOM[®]3-R7) preferably includes a switch (not shown) to switch the output signal on the set of ECG output connectors 150 from

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the ECG signal to a signal representative of the processed dZ/dt signal. For example, in the preferred embodiment, the output signal has a magnitude of 1 millivolt for each ohm per second of change in the electrical bioimpedance. A 5 signal of this magnitude is compatible with the range of input voltages that can be provided as inputs to a conventional ECG monitor.

The electrical bioimpedance monitor 104 further processes the differentiated electrical bioimpedance 10 information and the ECG information and calculates additional cardiovascular system information that is derived from the differentiated electrical bioimpedance information and the ECG. In particular, the electrical bioimpedance monitor 104 calculates the pre-ejection period (PEP), which 15 is measured between the onset of Q of the QRS complex of the ECG signal to the opening of the aortic valve), and the ventricular ejection time (VET), which is measured between the opening and the closing of the aortic valve. The ventricular ejection time is a direct measure of the 20 duration of the mechanical systole of the patient's heart. From these two calculated parameters, the electrical bioimpedance monitor 104 calculates the systolic time ratio (STR) as follows:

$$\text{STR} = \text{PEP}/\text{VET} \quad (4)$$

25 The calculated systolic time ratio is displayed and is provided as an output parameter from the electrical bioimpedance monitor 104.

The electrical bioimpedance monitor 104 derives the heart rate period (HRP) from the ECG signal. The heart 30 rate (HR) is derived from the heart rate period in a known manner (e.g., $\text{HR} = 60/\text{HRP}$). In addition, the heart rate period can be used in combination with the ventricular ejection time (VET) to calculate the ejection ratio (ER) as follows:

$$\text{ER}(\%) = (100 \times \text{VET})/\text{HRP} \quad (5)$$

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The electrical bioimpedance monitor 104 further calculates the thoracic fluid index (TFI) which is a value that represents the total resistance of the thorax to the flow of the high frequency, constant current injected into 5 the thorax as measured by the electrical bioimpedance monitor 104. Typical values for the thoracic fluid index vary from 20-33 ohms for male adults and 27-48 ohms for female adults and children.

The electrical bioimpedance monitor 104 calculates the ejection velocity index (EVI) which is the maximum value of 10 the rate of change of thoracic impedance change (i.e., $EVI = (dZ/dt)_{max}$) during the systolic upstroke. The ejection velocity index corresponds to the peak ejection velocity and the peak flow in the descending thoracic 15 aorta, and is directly related to the heart's contractility when it is normalized by the thoracic fluid index. The peak ejection velocity is measured in centimeters per second and the peak flow is measured in milliliters per second. The ejection velocity index represents these two 20 parameters in ohms per second. Because of the variability of the thoracic fluid index during a long range therapeutic procedure, the ejection velocity index alone is generally not usable to assess changes in a patient's inotropic state. Thus, the exemplary electrical bioimpedance monitor 25 104 (i.e., the NCCOM[®] 3-R7) calculates the index of contractility (IC) as the ratio of the ejection velocity index to the thoracic fluid index (i.e., $IC = EVI/TFI$). The index of contractility is displayed and is provided as 30 an output parameter from the electrical bioimpedance monitor 104.

The electrical bioimpedance monitor 104 calculates, displays and provides as an output signal on the serial data line 132 a digital output signal that represents the stroke volume (SV) of the patient's heart. The stroke 35 volume is calculated from the above-described parameters as follows:

$$SV = VEPT \times VET \times (EVI/TFI) = VEPT \times VET \times IC \quad (6)$$

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where VEPT is the physical volume of the electrically participating tissue in the thorax in milliliters. The parameter VEPT is calculated as $VEPT = (L^3/4.25)$, where L is the equivalent thoracic length in centimeters that is derived from the patient's height and body weight which are entered as input parameters by the clinician. Since stroke volume is a function of body mass, in most diagnostic and therapeutic procedures a normalized stroke index (SI) is desirable. The stroke index is determined by dividing the stroke volume by the patient's body surface area, calculated from the patient's height and weight, to obtain the stroke index normalized by body surface area, or by dividing the stroke volume by the patient's weight to obtain the stroke index normalized by weight.

The electrical bioimpedance monitor 104 calculates, displays and provides as a digital output signal the cardiac output (CO) in liters per minute. The cardiac output is calculated from the stroke volume and the heart rate as follows:

$$CO = SV \times HR \quad (7)$$

Cardiac output expresses the perfusion capability of the patient's heart. The resting cardiac output of a patient is a function of the patient's body mass. In order to be able to compare the adequacy of oxygen delivery of individuals of different body masses, the cardiac output is preferably normalized by body surface area or body weight to obtain the cardiac index (CI). The cardiac index by body surface area (CI_{BSA}) is obtained by dividing the cardiac output by the calculated body surface area derived from the height and weight parameters input by the clinician. The cardiac index by weight (CI_{weight}) is calculated by dividing the cardiac output by the patient's weight. The electrical bioimpedance monitor 104 selectively provides either the cardiac output or one of the two cardiac indices as a display and output parameter.

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Another parameter that is calculated, displayed and provided as an output is the peak flow (PF) which is calculated from the thoracic volume VEPT and the index of contractility IC as follows: ..

$$PF = VEPT \times IC \times \text{CONSTANT} \quad (8)$$

where CONSTANT is a dimensionless constant that is derived empirically. For example, in exemplary adult patients the constant is approximately 2.0. Peak flow represents the highest rate of left-ventricular volumetric delivery during the ejection phase of the cardiac cycle in milliliters per second. Peak flow is linked directly to the ejection phase contractility of the heart and as such is dependent on volemic status. Peak flow is one parameter that describes left ventricular performance. Alternatively, the electrical bioimpedance monitor 104 calculates, displays and outputs the peak flow index (PFI) which is the peak flow normalized by body surface area or body weight, depending upon which of the two indexing systems is selected.

The electrical bioimpedance monitor 104 also calculates, displays and provides as a digital output signal the ejection fraction (EF) which is calculated from the ratio of the pre-ejection period PEP to the ventricular ejection time VET. The ejection fraction is typically expressed as a percentage. The calculation is performed internally to the electrical bioimpedance monitor 104 in accordance with the following equation:

$$EF = 0.84 - (0.64 \times (PEP/VET)) \quad (9)$$

where the two constants have been derived empirically. The ejection fraction represents the volumetric emptying efficiency of the left ventricle, and thus represents the percentage of total volume contained in the ventricle just before the beginning of the systolic phase.

The electrical bioimpedance monitor 104 further calculates, displays and outputs the end-diastolic volume (EDV) which is volume of blood remaining in the heart at the end of the diastolic portion of the cardiac cycle and

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is calculated as the stroke volume divided by the ejection fraction. In other words:

$$\text{EDV} = \text{SV}/\text{EF} \quad (10)$$

where EDV is in milliliters. The end-diastolic volume is 5 preferably indexed by body surface area or body weight for comparison between patients. The indexed end-diastolic volume is referred to as the end-diastolic index (EDI) and is calculated as:

$$\text{EDI}_{\text{BSA}} = \text{EDV}/\text{BSA} \quad (11a)$$

$$\text{EDI}_{\text{WEIGHT}} = \text{EDV}/\text{WEIGHT} \quad (11b)$$

where EDI_{BSA} is in milliliters per square meter, and where $\text{EDI}_{\text{WEIGHT}}$ is in milliliters per kilogram.

The inotropic state of the left ventricle of the patient's heart (i.e., its contractile state), represented 15 by the index of contractility (IC), is dependent upon the fluid volume, the preload of the heart and the afterload of the heart. In contrast, the initial acceleration of the blood from the left ventricle of the heart takes place in the first 10-20 milliseconds after the aortic valve opens 20 and is related to the left ventricular impulse. The initial acceleration is substantially less load dependent and is thus more closely defines the inotropic state of the patient's vasculature system. As discussed above, the dZ/dt signal in ohms per second is processed by the 25 electrical bioimpedance monitor 104 as an ohmic image of blood flow (milliliters per second) and blood velocity (centimeters per second). The maximum rate of change of dZ/dt (i.e., d^2Z/dt^2_{max}) represents the ohmic counterpart of the acceleration of the blood. This parameter divided 30 by the thoracic fluid index (TFI) is calculated and displayed as the acceleration index (ACI). In other words, $\text{ACI} = d^2Z/dt^2_{\text{max}}/\text{TFI}$. The acceleration index is also provided as a serial data output parameter on the serial data line 130.

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The electrical bioimpedance monitor 104 of the preferred embodiment of the apparatus of the present invention calculates the foregoing parameters and displays selected ones of the parameters on a display panel (not shown) that is included as part of the electrical bioimpedance monitor 104. Furthermore, the calculated parameters are provided as serial output signals on the serial output connector 130 and thus as inputs to the computer 140 via the serial data line 132. In the exemplary electrical bioimpedance monitor 104 described herein (i.e., the NCCOM®3-R7), the output signals on the serial output connector 130 are provided in conventional RS-232 format at 9600 baud. Preferably, the output data format is as illustrated in Figure 5, with each character of data comprising a start bit, seven data bits, a parity bit (set to provide even parity in the preferred embodiment), and two stop bits. Other suitable formats can be used. It should be understood that the preferred format for the transmitted data is the standard ASCII codes for the numeric characters and the punctuation.

In the preferred embodiment incorporating the NCCOM®3-R7, the parameters can be provided as output signals in at least two different formats referred to as the FAST mode and the SLOW mode. In the slow mode, the electrical bioimpedance monitor 104 transmits eleven of the parameters described above in sequence, a character at a time, and outputs the calculated parameters on the serial data line 132 once for every sixteen heart beats. The electrical bioimpedance monitor 104 preferably outputs the average values of the parameters over the sixteen heartbeats. For example, in one exemplary embodiment, the following format for the transmission of the SLOW mode parameters is used:

:CO SV EDV PF EF HR TFI IC ER STR ACI HOUR:MIN

where the first eleven parameters are defined as discussed above, and HOUR and MIN are the twenty-four hour time of day entered into the electrical bioimpedance monitor 104

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and updated in accordance with a real-time clock within the electrical bioimpedance monitor 104. Preferably, the hour and minute information is transmitted only once every minute rather than every transmission. The first colon in
5 the transmission is used to indicate the beginning of a transmission sequence. Other delimiters could of course be used. The first colon can be distinguished from the colon between the hour and minute portion of the time portion as being preceded by a space rather than a number. Thus, the
10 computer 140 can readily use the first colon to synchronize with the serial data from the electrical bioimpedance monitor 104. Preferably, the data is output from the electrical bioimpedance monitor 104 as a series of digits only. The dimensions and the expected ranges are known by
15 the software algorithms in the computer 140. It should be understood that the transmitted data comprises numeric data, which may include a decimal point, separated by blank spaces (hexadecimal 20), and delimited by the colons.

Alternatively, the SLOW mode parameters are output as
20 follows:

:CI SI EDI PFI EF HR TFI IC ER STR ACI HOUR:MIN

wherein the cardiac index (CI), the stroke index (SI), the end-diastolic index (EDI) and the peak flow index (PFI) are substituted for their respective unindexed values. The
25 indexing can be in accordance with body surface area or weight, as discussed above.

Preferably, additional patient information, such as the patient's sex, identification number, height, weight, VEPT (thoracic volume), and calculated body surface area (BSA), are also transmitted from the electrical bioimpedance monitor 104 to the computer 140. Preferably, the additional patient information is transmitted only once at the beginning of the data transmission as these parameters should not change for a patient during a diagnostic session.
30

In the FAST mode, the calculated parameters are transmitted once for each heart beat. Because of the
35

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transmission rates and the time required to perform the calculations, in the FAST mode, only six of the foregoing parameters are transmitted. For example, the following exemplary format is used for unindexed parameters:

5 : CO SV EDV PF EF HR HOUR:MIN

Alternatively, the indexed parameters can be transmitted as follows:

: CI SI EDI PFI EF HR HOUR:MIN

10 As with the SLOW mode, the hour and minute information is preferably transmitted only once per minute rather than in every transmission. Furthermore, the other patient parameters and identification information, discussed above, are preferably transmitted once at the beginning of diagnostic session.

15 Additional information regarding the operation of the exemplary NCCOM®3-R7 electrical bioimpedance monitor in sensing the electrical bioimpedance changes and calculating the above-described parameters can be found in "NCCOM®3-R7 CARDIOVASCULAR MONITOR OPERATOR'S MANUAL," available from
20 BoMed® Medical Manufacturing Ltd., 5 Wrigley Street, Irvine, California 92718.

One additional input to the computer 140 is required in order to complete the system of the present invention. As discussed above, the mean arterial blood pressure (MAP) 25 is a factor in the determination of the appropriate therapeutic procedure to return the patient to a normal range of conditions for the patient's vasculature system. The mean arterial blood pressure can be provided as an input by a number of different methods. One of the simplest. 30 and most straight forward apparatus and methods for inputting the mean arterial blood pressure to the computer 140 is to measure the mean arterial blood pressure using a conventional occlusive cuff to determine the systolic and

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diastolic pressures, calculating the mean arterial blood pressure in accordance with the Equation 1, above as:

5 MAP = $\frac{\text{SYSTOLIC} - \text{DIASTOLIC}}{3} + \text{DIASTOLIC}$ (1)

The result of the calculation is then entered into the computer 140 using the keyboard 142. This combination of apparatus and method has the disadvantage of requiring manual input from a clinician with the accompanying 10 possibility of introducing error into the computer 140. Furthermore, this combination of method and apparatus does not lend itself to automatic monitoring of the condition of the patient's vasculature system. Thus, it is preferable that an automated system be used for measuring the patient's 15 mean arterial blood pressure and providing it as an input to the computer 140.

A number of systems are available for automatically measuring a patient's blood pressure and providing it as an input to the computer 140. One such system is described in 20 United States Patent No. 4,677,984, which is incorporated herein in its entirety. The system disclosed in United States Patent No. 4,677,984 is illustrated in simplified form in Figure 6. As illustrated, the system includes an automatic cuff pressure generator 200 controlled by a 25 processor 204. The pressure is selectively coupled to an occlusive cuff 210. The system further includes an ECG monitoring device 212 to sense the occurrence of an R-wave in the ECG signal of the patient. The system includes a pressure transducer 214 detects transitions in the pressure 30 in the occlusive cuff 210 caused by the passage of a bolus of blood beneath the cuff 210 when the arterial pressure exceeds the cuff pressure during a cardiac cycle. The transitions are timed with respect to the occurrence of the R-wave of the ECG to maintain a record of the pressure 35 transitions as the pressure on the occluding bladder is systematically decreased or increased. The recorded pressure transitions and times are used to reproduce the arterial blood pressure waveform from which the mean

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arterial blood pressure can be calculated. In the present invention, the processor 204 of Figure 6 provides an output signal representing the mean arterial blood pressure that is provided as an input signal to the computer 140 of 5 Figure 4. This connection is shown as a dashed line 220 in Figures 6 and 4. In a fully integrated system, the computer 204 used to record the pressure transitions and times advantageously can be the same computer 140 that receives the serial data information from the electrical 10 bioimpedance monitor 104.

The pressure can also be measured using electrical bioimpedance techniques as set forth in allowed U.S. Patent Application Serial No. 111,699, filed on October 21, 1987, and assigned to the assignee of this application, and which 15 is incorporated herein by reference. This system is illustrated in part in Figure 7. As illustrated in Figure 7, the automatic blood pressure measuring system includes a pair of electrical bioimpedance measuring devices, one of which is the electrical bioimpedance monitor 104, disclosed 20 and described above. A second electrical bioimpedance measuring device 230 is connected to a set of current injecting electrodes 232a and 232b and a set of current sensing electrodes 234a and 234b on the calf of the patient's leg that defines a second body segment for 25 bioimpedance sensing. The second electrical bioimpedance device 230 can be a much simpler device than the electrical bioimpedance monitor 104, as it is only necessary to detect the peak on the change in the electrical bioimpedance in the patient's leg. As described in U.S. Patent Application 30 Serial No. 111,699, a computation circuit 240 receives the dZ/dt output signals from the electrical bioimpedance monitor 104 and the electrical bioimpedance measuring device 230 and calculates the time delay (i.e., the arterial pulse propagation delay) between the peaks in the 35 two dZ/dt signals. The computation circuit 240 uses the measured time delay to determine the mean arterial blood pressure therefrom. As set forth in U.S. Patent

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Application Serial No. 111,699, the time delay and the spacing of the second body segment of the leg from the first body segment of the patient's thorax provide sufficient information from which the mean arterial blood pressure 5 (MAP) can be calculated. The computation block 240 advantageously provides the calculated mean arterial blood pressure as an output on a line 250 which is connected to an input to the computer 140. Thus, the mean arterial blood pressure is provided as an input to the computer 140. It 10 should be understood that the computation block 240 can advantageously be a microprocessor or other programmable computation device. Although shown as a single serial data line 250, it should be understood that the data can be transmitted from the computation block 240 to the computer 140 via a parallel data bus, for example.

Other known automatic or manual methods and apparatus can be used to measure the mean arterial blood pressure and provide it as an input to the computer 140 for use in calculating the therapeutic information, as will be 20 described hereinafter.

The computer 140 uses the data information from the electrical bioimpedance monitor 104 and the mean arterial blood pressure provided as a data input from the keyboard 142 or from the automated system of Figure 6 or Figure 7. 25 An exemplary flow chart for the operation of the computer 140 is illustrated in Figure 8.

Description of the Flow Chart of the Computer Algorithms

As illustrated in Figure 8, the computer 140 is programmed with an algorithm 300 that includes an entry 30 block 310 wherein the program begins. Thereafter, the algorithm enters a first activity block 314 in which the program is initialized. The program requests various parameters from the clinician including the patient's name and other identification information. Thereafter, the 35 algorithm enters a second activity block 318 in which the computer inputs data that represents the mean arterial blood pressure (MAP). The MAP data can be entered from the

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keyboard 142 when the MAP is provided by manual methods and apparatus. Alternatively, the MAP can be provided as a direct digital input from the automated blood pressure measuring system of Figure 6 or the automated blood pressure measuring system of Figure 7, as discussed above. After entering and storing the MAP, the computer algorithm enters a decision block 322 wherein the algorithm monitors waits for an interrupt indicating that new data has begun to arrive on the serial data input lines from the electrical bioimpedance monitor 104, that the clinician has entered a command from the keyboard 142, or that other real-time activities have occurred that must be handled, such as the clock interrupt internal to the computer 140. So long as no interrupt has occurred, the algorithm will reenter the decision block 322.

When an interrupt occurs, the algorithm will enter a process block 330 wherein it processes the interrupt and branches to the appropriate routine determined by the nature of the interrupt. The various routines are shown as three generalized routines. If the interrupt is an internal computer interrupt, such as the real-time clock interrupt, the algorithm enters an activity block 334 wherein the internal computer interrupts are processed in known conventional manners. These interrupts are handled in a conventional manner by the disk operating system (DOS) or other system level programs provided with the computer 140. Thus, the handling of these interrupts is transparent to the algorithm itself and control is returned from the activity block 334 back to the decision block 322 where the algorithm awaits the next interrupt.

If the interrupt is a keyboard entry interrupt, the algorithm enters an activity block 340 wherein the data entered via the keyboard 142 is provided as an input to the algorithm for further processing. For example, the data can indicate that the clinician desires to re-initialize the algorithm. Thus, a path is illustrated that returns the algorithm control back to the first activity block 314

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wherein the algorithm is re-initialized. The data can also indicate an update of the patient's mean arterial blood pressure. Thus, a path is illustrated from the activity block 340 to the second activity block 318 wherein the MAP 5 is updated. It should be understood that in the embodiment of Figure 6 or the embodiment of Figure 7, wherein the MAP is generated automatically, an interrupt from the external computer 210 (Figure 6) or the computer 220 (Figure 7) causes the computer 140 to input the MAP data from the 10 corresponding external computer.

The keyboard entry can also be a request to terminate the program. Thus, a path is provided from the keyboard entry activity block 340 to a program termination block 344. Other keyboard entries could of course envisioned. 15 However, rather than attempt to enumerate all possible entries, a path is illustrated from the keyboard entry activity block 340 back to the decision block 322 wherein the algorithm waits for the next interrupt.

The third general type of interrupt is generated when 20 serial data inputs are received from the electrical bioimpedance monitor 104. As set forth above, the electrical bioimpedance monitor 104 periodically outputs the calculated parameters of the vasculature system to the computer 140. When the serial data is received by the 25 computer 140, an interrupt is generated and the algorithm enters an activity block 350 wherein the computer inputs the data from the electrical bioimpedance monitor 104. Thereafter, the algorithm enters an activity block 354 30 wherein the computer 140 calculates the systemic vascular resistance index (SVRI) in accordance with the Equation (2) as follows:

$$\text{SVRI} = \frac{(\text{MAP} - \text{CVP}) \times 80}{\text{CI}} \quad (2)$$

35. As discussed above, CVP is the central venous pressure which is estimated to be approximately 3 Torr. The cardiac index (CI) is one of the parameters received on the serial data line 132 from the electrical bioimpedance monitor 104.

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The dimensions of SVRI resulting from the above calculation is in dyn·sec/cm⁵m², also referred to herein as fluidic ohms per square meter (F.Ohms/m²).

After calculating the SVRI, the algorithm enters an 5 activity block 358 wherein the computer 140 calculates the left cardiac work index (LCWI) in accordance with Equation (3) as follows:

$$LCWI = (MAP - PAOP) \times CI \times 0.0144 \text{ kg} \cdot \text{m/m}^2 \quad (3)$$

As discussed above, PAOP is pulmonary artery occluded 10 pressure in Torr, CI is the cardiac index in liters/min/m², and 0.0144 is a constant of proportionality. As further discussed above, in the typical patient, the PAOP will be approximately 6 Torr, and this value may be ordinarily assumed without subjecting the data to any significant 15 error. However, a patient's actual PAOP can vary sufficiently to justify determination of the actual PAOP value for use in Equation (3) under conditions of pump failure. In such a case, the actual PAOP is entered via the keyboard 142 by the clinician. The dimensions of LCWI 20 resulting from the above calculation are in kilograms per square meter (kg·m/m²).

After calculating the left cardiac work index, the algorithm enters an activity block 370 wherein the computer 140 branches to a selected one of an activity block 374 or 25 an activity block 378 wherein the computer provides a visual display of the calculated data. Two primary alternative data displays are advantageously provided in the preferred embodiment of the present invention. The selection of which type of display to provide is one of the 30 selections that can be entered via the keyboard when the computer 140 is in the activity block 340. Other types of displays can also be advantageously provided. After providing an updated display as an output in either the activity block 374 or the activity block 378, the algorithm 35 returns to the decision block 322 to await the next interrupt. Additional details regarding the two primary

-38-

types of displays generated in accordance with the present invention are illustrated in Figures 9 and 10, and are described hereinafter.

One of the two primary displays is provided when the computer enters the activity block 374. The display associated with the activity block 374 is illustrated in Figure 9. In Figure 9, the cardiovascular and hemodynamic data are displayed as a bar chart comprising a series of ten bar graphs. The bar chart of Figure 9 is referred to as the diagnostic chart as it allows the clinician to quickly review ten parameters reflecting the hemodynamic state of the patient's cardiovascular system.

In the exemplary display of Figure 9, the bar graphs are horizontal and the length of the bar graph in the horizontal direction represents the magnitude of the corresponding parameter.

As illustrated in Figure 9, the bar graphs are labeled with the abbreviations for each of the parameters, as introduced above. In addition, in order to assist the clinician in quickly perceiving the significance of parameter that is outside the indicated normal range, the bar graphs preferably include a translation of the various parameters into more readily understood terms. The cardiac index (CI) is referred to as the GLOBAL FLOW and has the dimensions of liters/min/m².

Four of the parameters relate to the pump performance. The stroke index (SI) is referred to as the PUMP PERFORMANCE and has the dimensions of milliliters/m². One modulator that affects pump performance is the end diastolic index (EDI) which is referred to as the PRELOAD and has the dimensions of milliliters/m². The index of contractility (IC) and the acceleration index (ACI) are both shown as CONTRACTILITY parameters. The index of contractility is dependent upon fluid volume and has the dimensions 1/sec. The acceleration index is dependent upon the inotropic state of the patient's vasculature system and has the dimensions of 1/sec². The systemic vascular resistance index (SVRI) is

-39-

referred to as the AFTERLOAD of the heart and has the dimensions of fluid ohms/m².

The left cardiac work index (LCWI) is referred to as the CARDIAC WORK and represents the amount of work the 5 heart has to expend in order to deliver the blood flow. The left cardiac work index has the dimensions of kg·m/m².

The ejection fraction (EF) is referred to as the PUMP EFFICIENCY and is expressed as a percentage.

In the preferred embodiments of the present invention, 10 the thoracic fluid index (TFI) from the NCCOM®3-R7 is inverted and displayed as thoracic fluid conductivity (TFC) (i.e., TFC = 1/TFI). The thoracic fluid conductivity has a normal range of 0.030 to 0.050 mhos (i.e., 1/ohms). In Figure 9, the thoracic fluid conductivity is referred to as 15 the THORACIC FLUIDS. By using the conductivity, increasing amount of fluids results in increased conductivity and thus results in a shift in the bar graph to the right. Thus, the clinician perceives an increase (movement to the right) of the bar graph as an increase in the patient's fluids.

20 The mean arterial blood pressure (MAP) is displayed as the lowermost bar graph in Figure 9 and is dimensioned in Torr.

As illustrated, the magnitude of each of the foregoing 25 parameters is displayed both as a numeric value and as a length on the corresponding bar graph. The bar graph for each of the parameters further includes a pair of lines perpendicular to the bar graph (i.e., a pair of vertical lines 380 and 382, as illustrated for the bar graph for the cardiac index) which delineate the range of "normal" values 30 for the parameter. (It should be understood that on a video display monitor, the vertical lines can be highlighted with a different color or brightness level so that they are more readily discernible.) For example, the bar graph for the cardiac index (CI) is shown as having the first vertical 35 line 380 at a magnitude of 2.8 liters/min/m², representing the lower limit of the "normal" range, and having the second vertical line at a magnitude of 4.2 liters/min/m²,

-40-

representing the upper limit of the "normal" range. Thus, a clinician can easily determine which of the parameters are outside the normal range. For example in Figure 9, it can be seen that the magnitudes of the systemic vascular
5 resistance index (SVRI) and the mean arterial blood pressure are greater than the normal ranges for those parameters, and the magnitudes of the cardiac index (CI) and the index of contractility (IC) are less the normal range. In contrast the remaining six parameters are within their normal ranges.

10 Preferably, the bar graphs representing the parameters are scaled so that the vertical lines for each of the bar graphs, with the exception of the mean arterial pressure bar graph, are vertically aligned with respect to each other, as illustrated in Figure 9, to assist the clinician
15 in quickly recognizing which of the parameters are above or below their respective "normal" ranges. Because of the large magnitude in the range of the mean arterial blood pressure, the vertical lines representing its "normal" limits are not aligned with the vertical lines of the other
20 parameters.

The heart rate (HR), the patient's height, patient's weight and patient's date of birth are displayed in the display format of Figure 9 as numeric parameters without corresponding bar graphs. The display format can also
25 include other patient identification information and data storage identification.

When the computer 140 enters the activity block 378, it provides the alternative primary display illustrated in Figure 10, which displays the hemodynamic status of the patient's cardiovascular system. Unlike the display of Figure 9, the display of Figure 10 provides an alphanumeric display of five of the above-described parameters, namely the cardiac index (CI), the mean arterial blood pressure (MAP), the left cardiac work index (LCWI), the systemic vascular resistance index (SVRI) and the heart rate (HR).
30
35

The display of Figure 10 is distinguished from the display of Figure 9 in that the cardiac Index (CI) and the

-41-

mean arterial blood pressure (MAP) are also displayed as a cartesian graph. The cardiac index is on the X-axis (i.e., the horizontal axis) and the mean arterial blood pressure is on the Y-axis (i.e., the vertical axis). The cartesian graph of Figure 10 generally corresponds to the graphs of Figures 1, 2 and 3, and has an ellipse 400 that represents the range of normal combinations of magnitudes of the cardiac index and the mean arterial blood pressure. In Figure 10, the ellipse 400 has a center 404 (i.e., the intersection of its major and minor axes) at a cardiac index of 3.5 liters/min/m², and at a mean arterial blood pressure of 92 Torr.

In addition to the ellipse 400, the cartesian graph of Figure 10 includes a first curve 410 and a second curve 414 (both shown as dotted lines) that intersect at the center 404 of the ellipse 400. The curve 410 represents the normal left cardiac work index (LCWI), which in the display of Figure 10 is equal to approximately 4.35 kg.m/m². The curve 414 represents the normal systemic vascular resistance index (SVRI), which in the display of Figure 10 is equal to approximately 2030 fluidic ohms per square meter.

The cartesian graph of Figure 10 further includes an indicator 420 that represents the patient's cardiac index and the patient's mean arterial blood pressure, and also represents the patient's left cardiac work index and systemic vascular resistance index. As illustrated for an exemplary patient having the parameters illustrated in Figures 9 and 10, the patient's cardiac index (CI) is 2.7 liters/min/m², which is below the normal range of values; and the patient's mean arterial blood pressure is 135 Torr which is considerably above the normal range of values. In addition, the patient's left cardiac work index (LCWI) is 5.0 kilograms per square meter, which is at the high end of the normal range for that parameter. The patient's systemic vascular resistance index (SVRI) is 3870 fluidic ohms/m², which is considerably greater than the normal range. By observing the position of the indicator 420 with

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respect to the ellipse 400 and with respect to the first curve 410 and the second curve 414, the clinician can readily perceive which of the four parameters differ from the normal values for the parameters.

- 5 In order to assist the clinician in quantitatively analyzing the displayed data, the display of Figure 10 further includes an alphanumeric display of the percentage deviation of the calculated left cardiac work index and the systemic vascular resistance index from the normal values
10 and indicates whether the parameters are greater than or less than the normal values. For example, in Figure 10, the left cardiac work index is approximately 15 percent below a normal value of approximately $4.35 \text{ kg} \cdot \text{m/m}^2$, which represents relative hypervolemia or relative hyperinotropy.
15 The systemic vascular resistance index is 91 percent above a normal value of approximately $2030 \text{ dyn} \cdot \text{sec/cm}^5 \text{m}^2$ (i.e., 2030 F.Ohms/m^2), which represents relative hypovolemia.

The cartesian graph display of Figure 10 is referred to as the therapeutic management chart. The clinician can 20 use the information displayed in the therapeutic management chart of Figure 10 in combination with the diagnostic chart of Figure 9 to determine a proper course of therapy, as discussed above in connection with Figures 1, 2 and 3. For example, the clinician will observe that the patient will 25 require therapy that increases the patient's arterial capacitance to reduce the systemic vascular resistance index. In addition, the patient will likely require therapy that increases either or both the patient's fluid volume or the patient's inotropy. For example, the 30 acceleration index (ACI) parameter in Figure 9 indicates that the patient's inotropic state is substantially normal. In contrast, the volume-dependent index of contractility (IC) parameter is below normal and indicates that the patient is hypovolemic. Thus, the proper therapy for the 35 exemplary patient having these parameters should be increase the patient's fluid volume. This is consistent

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with the bar graph of the thoracic fluid conductivity in Figure 9 which is at the low end of the normal range.

As discussed above, the end goal of the therapy is not always necessarily within the normal ranges of the displayed parameters. For example, a patient recovering from major surgery or certain illnesses may require additional oxygen to assure successful recovery. The clinician can use the displays of Figures 9 and 10 to determine a course of treatment in which the cardiovascular system is operated with parameters outside the normal range to enhance the patient's recovery. For example, it is preferable that a post-surgical course of therapy include a modality to cause the patient to be relatively hypervolemic to increase the oxygen-carrying capability of the patient's system. In preferred embodiments of the present invention, the clinician can select an alternative display mode in which the "normal" cardiac index, systemic vascular resistance index and left cardiac work index are adjusted to set a new goal for the patient's volume/ inotropy and the patient's arterial capacitance in accordance with results of the study by W.C. Shoemaker. In other words, a goal is set to increase the oxygen perfusion of the tissues. This is illustrated in Figures 11 and 12 which illustrate two exemplary cartesian displays for the same patient.

In Figure 11, the above-described normal ranges for the cardiac index, the systemic vascular resistance index and the left cardiac work index are used to define the ellipse 400, the first curve 410 and the second curve 414. The measured parameters are displayed alphanumerically to the left of the graph and the indicator 420 is located to show that the blood pressure is low, the cardiac index is low, the left cardiac work index is low (indicating either relative hypovolemia and/or relative hypoinotropy), and that the systemic vascular resistance index is "normal" (indicating normocapacitance). Thus, the indicated therapy would be to increase the volume and/or the inotropy. The

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location of the indicator 420 on the normocapacitance curve does not indicate any therapy related to the capacitance.

Figure 11 should be contrasted with Figure 12 which illustrates the same parameters for a patient recovering from surgery, or the like. The "normal" values for the cardiac index, the systemic vascular resistance index and the left cardiac work index have been adjusted upward in Figure 12 to represent a therapeutic goal that will result in increased oxygen perfusion of the tissues. For example, the normal range of the cardiac index (CI) is shown as being approximately 3.8 to 5.2 liters/min/m² rather than 2.8 to 4.2 liters/min/m². Similarly, a curve 410' for the left cardiac work index (LCWI), representing the "normovolemia/normoinotropic," condition has been shifted to approximately 5.55 kg·m/m²; and a curve 414' for the systemic vascular resistance index, representing the "normocapacitance" condition has been shifted to approximately 2690 F·Ohms/m² (2690 dyn·sec/cm⁵m²). Thus, as illustrated by the location of the indicator 420' in Figure 12, the post-operative patient is 55 percent relatively hypovolemic and the therapeutic modality to expand the patient's fluid volume should be increased with respect to the corresponding treatment for the normal goals illustrated in Figure 11. At the same time, the patient should be vasodilated in response to the 26 percent relative hypocapacitance according to the new system vascular resistance index goal in order to increase the intravascular space for the acceptance of additional fluids.

As set forth above, the electronic system of the present invention preferably includes the printer 145. The printer is preferably capable of printing graphic images of the screen displays of Figures 9 and 10 to provide a permanent record of the screen displays so that they may be compared to analyze the results of a course of therapy over a period of time. In addition, the computer 140 preferably includes long term data storage capabilities (i.e., a hard disk drive and/or a floppy disk drive) so that the data

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collected during a diagnostic session can be saved and displayed contemporaneously with the data collected during a current diagnostic session. Thus, the clinician can observe the results of the previously prescribed therapy and modify
5 the therapy, as needed, in order to achieve the desired end results.

Although this invention has been described in terms of certain preferred embodiments, other embodiments that are apparent to those of ordinary skill in the art are also
10 within the scope of this invention. Accordingly, the scope of the invention is intended to be defined only by reference to the appended claims.

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CLAIMS:

1. A system for determining the hemodynamic state of a mammal, characterized by:

5 means (104) for measuring the cardiac index of the mammal and providing the cardiac index as a digital output signal;

means (204) for measuring the mean arterial blood pressure (MAP) of the mammal;

10 a computational system (140) that receives said digital output signal representing said cardiac index as a first input and that receives a second input representing said mean arterial blood pressure, said computational system calculating the left cardiac work index (LCWI) and the systemic vascular resistance (SVRI) of the mammal in accordance with the following equations:

$$LCWI = (MAP - PAOP) \times CI \times K$$

$$SVRI = ((MAP - CVP) \times L) / CI$$

20 wherein PAOP represents the pulmonary occluded pressure of the mammal and CVP represents the central venous pressure of the mammal, said PAOP and said CVP being constants that are provided as additional inputs to the computational system; and wherein K and L are predetermined constants, said computational system providing said calculated LCWI and SVRI as human readable output data, said computational system (140) further providing a display of said calculated LCWI and SVRI as graphs.

25 30 2. The system as defined in Claim 1, wherein said means (104) for measuring the cardiac index of the mammal is an electrical bioimpedance monitor (104) that senses changes in the electrical bioimpedance of the mammal during each cardiac cycle and that calculates the cardiac index of the mammal from said sensed changes.

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3. The system as defined in Claim 1, wherein said graphs include a cartesian graph with the cardiac index as one axis and the mean arterial blood pressure on the other axis, said graph further including curves (410, 410', 414, 414') illustrating the normal values of LCWI and SVRI and an indicator (420, 420') showing the location of the calculated values of LCWI and SVRI with respect to the curve (410, 410', 414, 414').
- 5 4. The system as defined in, Claim 3, further including a display of percent deviation of said calculated LCWI and SVRI from said normal values of LCWI and SVRI.
- 10 5. A method of achieving a preselected hemodynamic state in a subject mammal, characterized by the steps of:
- 15 (a) determining the subject's mean arterial pressure (MAP);
- (b) measuring the subject's cardiac index (CI);
- (c) determining the subject's left cardiac work index (LCWI) utilizing the measured MAP and CI values according to the formula:
- 20
$$\text{LCWI} = (\text{MAP} - \text{PAOP}) \times \text{CI} \times K$$
 wherein PAOP represents pulmonary artery occluded pressure and K is a constant;
- 25 (d) determining the subject's systemic vascular resistance index utilizing the measured MAP and CI values according the formula:
- 30
$$\text{SVRI} = \frac{(\text{MAP} - \text{CVP}) \times L}{\text{CI}}$$
 wherein SVRI represents the systemic vascular resistance index, CVP is central venous pressure and L is a constant; and
- 35 (e) administering a therapeutic dose of a pharmacologically active material for altering the LCWI and SVRI values to achieve in the subject a preselected hemodynamic state.

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6. A method of achieving a preselected hemodynamic state as defined in Claim 5, wherein the subject is an adult human.

5 7. A method of achieving a preselected hemodynamic state as in Claim 6, wherein the preselected hemodynamic state comprises a systemic vascular resistance index of approximately 2030 dyn.sec/cm^{5m2}, and a left cardiac work index of approximately 4.35 kg.m/m².

10 8. A method of achieving a preselected hemodynamic state as defined in Claim 7, wherein the pharmacologically active material comprises a vasodilator if the systemic vascular resistance index is greater than about 2030 dyn.sec/cm^{5m2}.

15 9. A method of achieving a preselected hemodynamic state as defined in Claim 7, wherein the pharmacologically active material comprises a vasoconstrictor if the systemic vascular resistance index is less than about 2030 dyn.sec/cm^{5m2}.

20 10. A method of achieving a preselected hemodynamic state as defined in Claim 5, wherein the patient is an adult human and the preselected hemodynamic state comprises a systemic vascular resistance index within the range of from about 1700 to about 2650 dyn.sec/cm^{5m2}.

25 11. A method of achieving a preselected hemodynamic state as defined in Claim 5, wherein the patient is an adult human and the preselected hemodynamic state comprises a left cardiac work index within the range of from about 3.3 to about 5.3 kg.m/m².

30 12. A method of achieving a preselected hemodynamic state as defined in Claim 5, wherein the patient is a neonatal infant human and the preselected hemodynamic state comprises a systemic vascular resistance index within the range of from about 950 to about 1500 dyn.sec/cm^{5m2}.

35 13. A method of achieving a preselected hemodynamic state as defined in Claim 5, wherein the patient is a

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neonatal human infant and the preselected hemodynamic state comprises a left cardiac work index within the range of from about 2.5 to about 4.0 kg·m/m²

14. A method of determining and correcting deviations
5 from normovolemia in a subject mammal, characterized by the steps of:

(a) determining the subject's mean arterial pressure (MAP);

(b) measuring the subject's cardiac index (CI);

10 (c) determining deviation from normovolemia by utilizing the measured values of MAP and CI according to the formula:

15 deviation = $\frac{(MAP - PAOP) \times CI \times K}{4.35 \text{ kg} \cdot \text{m/m}^2}$

wherein PAOP is the pulmonary artery occluded pressure and K is a constant; and

20 (d) increasing fluid volume if deviation is less than 1.0, and decreasing fluid volume if deviation is greater than 1.0.

15. A method of achieving a preselected hemodynamic state in a mammal, characterized by the steps of:

determining mean arterial pressure in the mammal;

measuring cardiac index in the mammal;

25 determining a first deviation, if any, from a preselected volemic state;

determining a second deviation, if any, from a preselected capacitive state; and

30 administering a therapeutic dose of at least one pharmacologically active material for altering the first and second deviations to achieve a preselected hemodynamic state.

16. A method of achieving a preselected hemodynamic state as defined in Claim 15, wherein the preselected 35 volemic state is normovolemic.

-50-

17. A method of achieving a preselected hemodynamic state as defined in Claim 15, wherein the preselected capacitive state is normocapacitive.

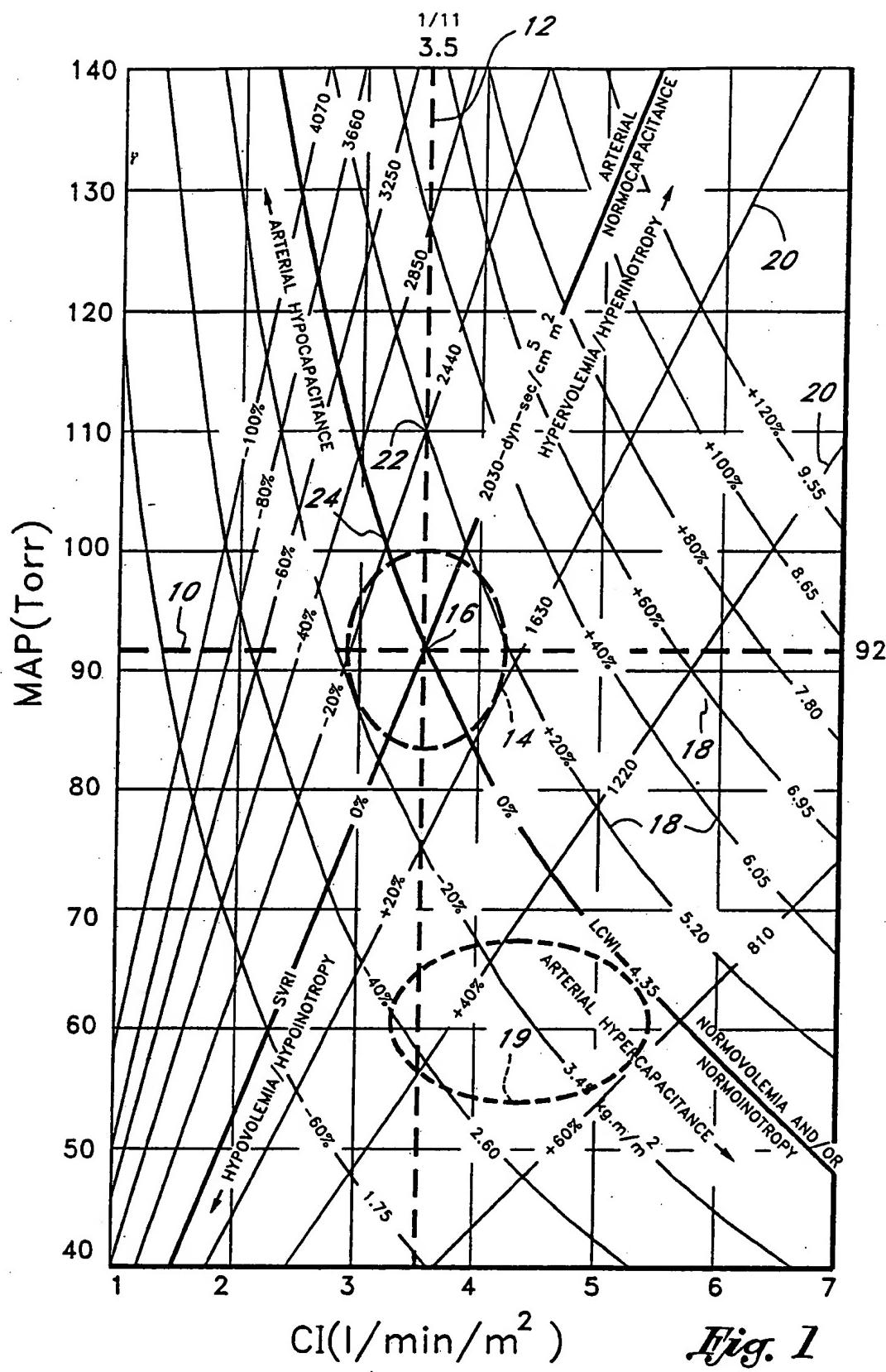
5 18. A method of achieving a preselected hemodynamic state as defined in Claim 15, wherein the preselected hemodynamic state comprises normovolemia, normoinotropy and arterial normocapacitance.

10 19. A method of achieving a preselected hemodynamic state as defined in Claim 18, wherein the preselected hemodynamic state comprises a mean arterial pressure of from about 84 to about 100 Torr.

15 20. A method of achieving a preselected hemodynamic state as defined in Claim 16, wherein the volemic state is measured as the left cardiac work index and ranges from approximately 3.3 to 5.3 kg·m/m².

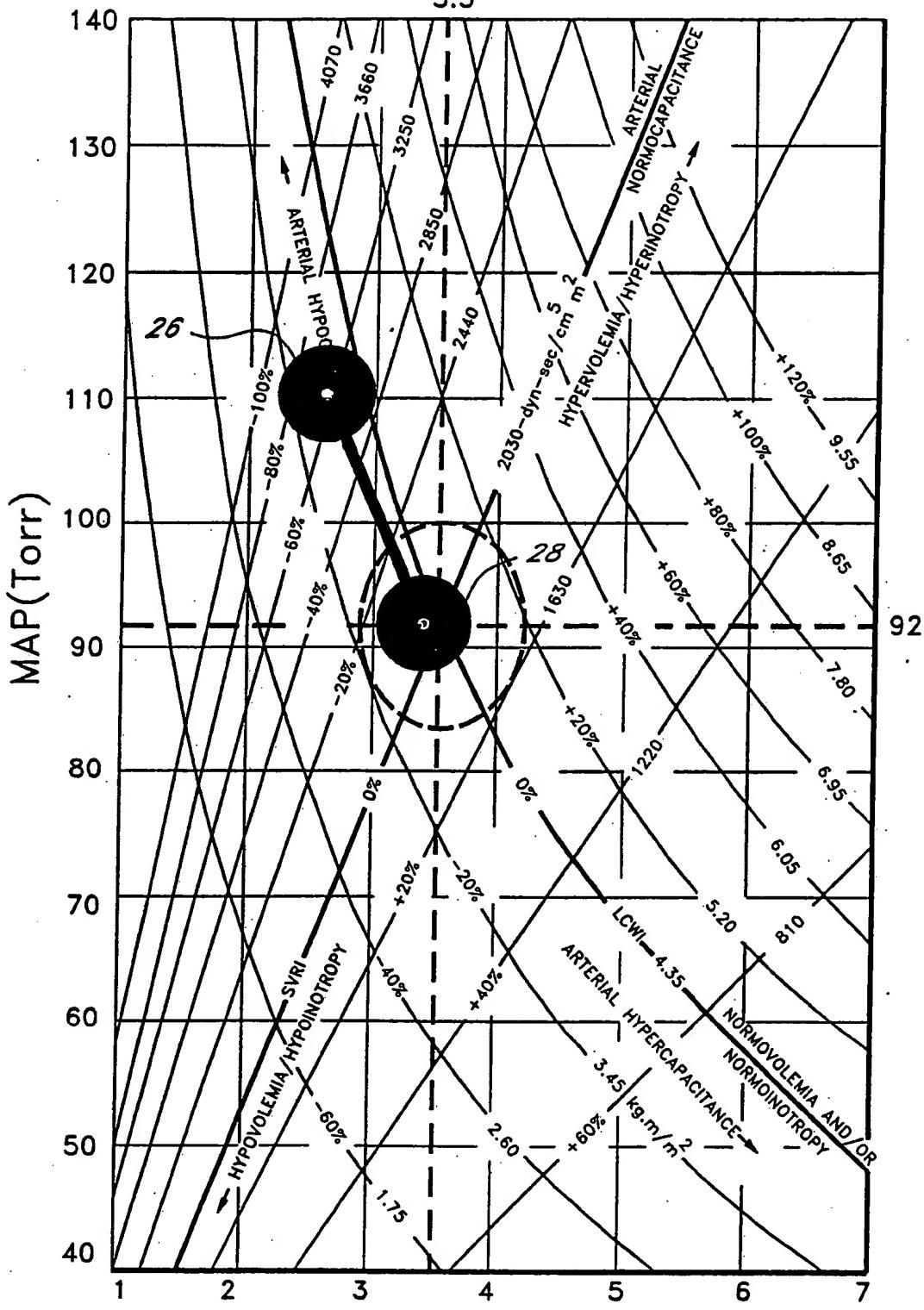
20 21. A method of achieving a preselected hemodynamic state as defined in Claim 15, further comprising the step, prior to the administering step, of selecting a pharmacologically active material for reducing the deviation from the preselected volemic state.

25 22. A method of achieving a preselected hemodynamic state as defined in Claim 15, wherein the mammal is a human adult in postoperative recovery and the preselected hemodynamic state comprises normotension and hyperdynamic global blood flow.

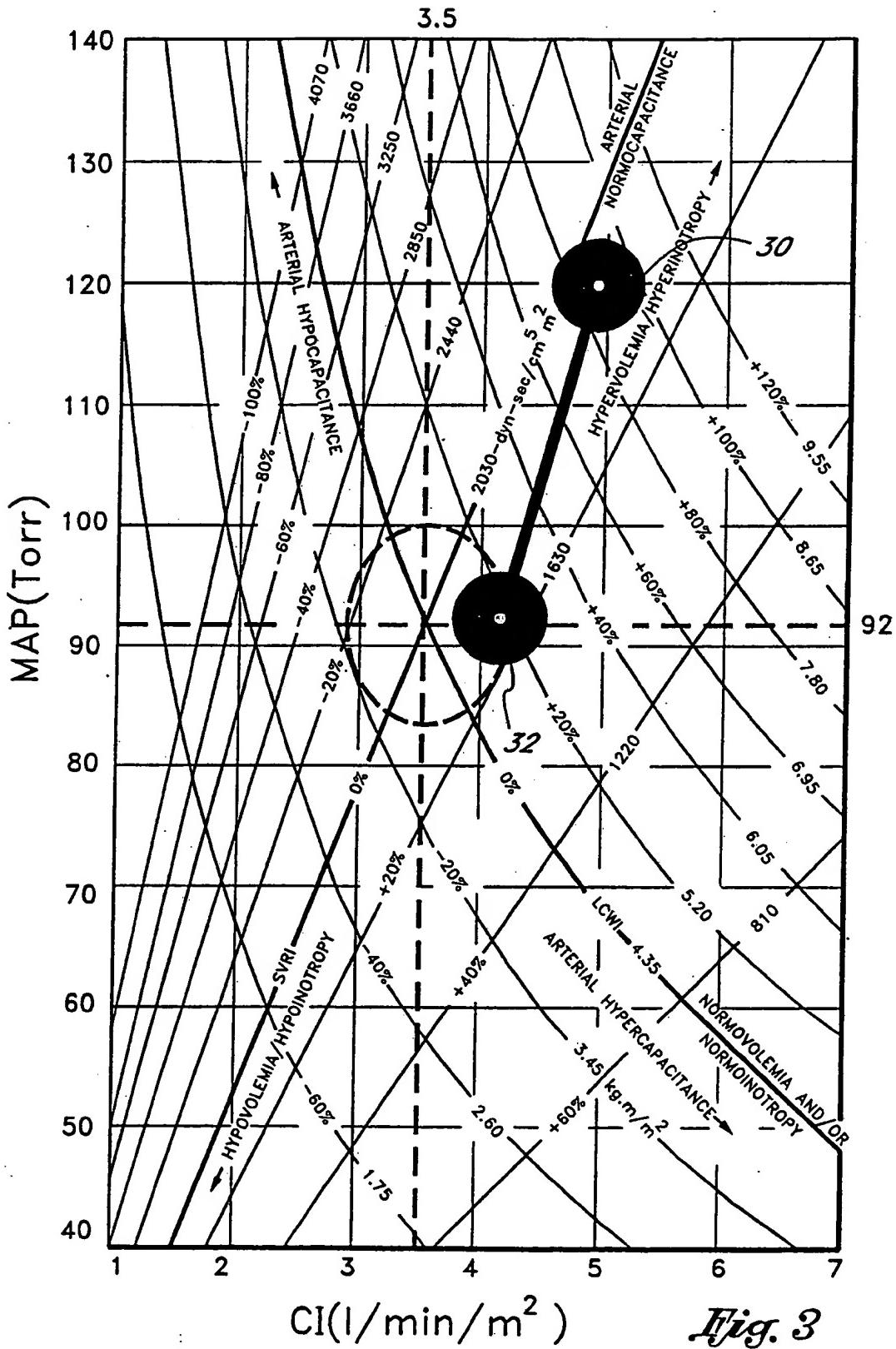


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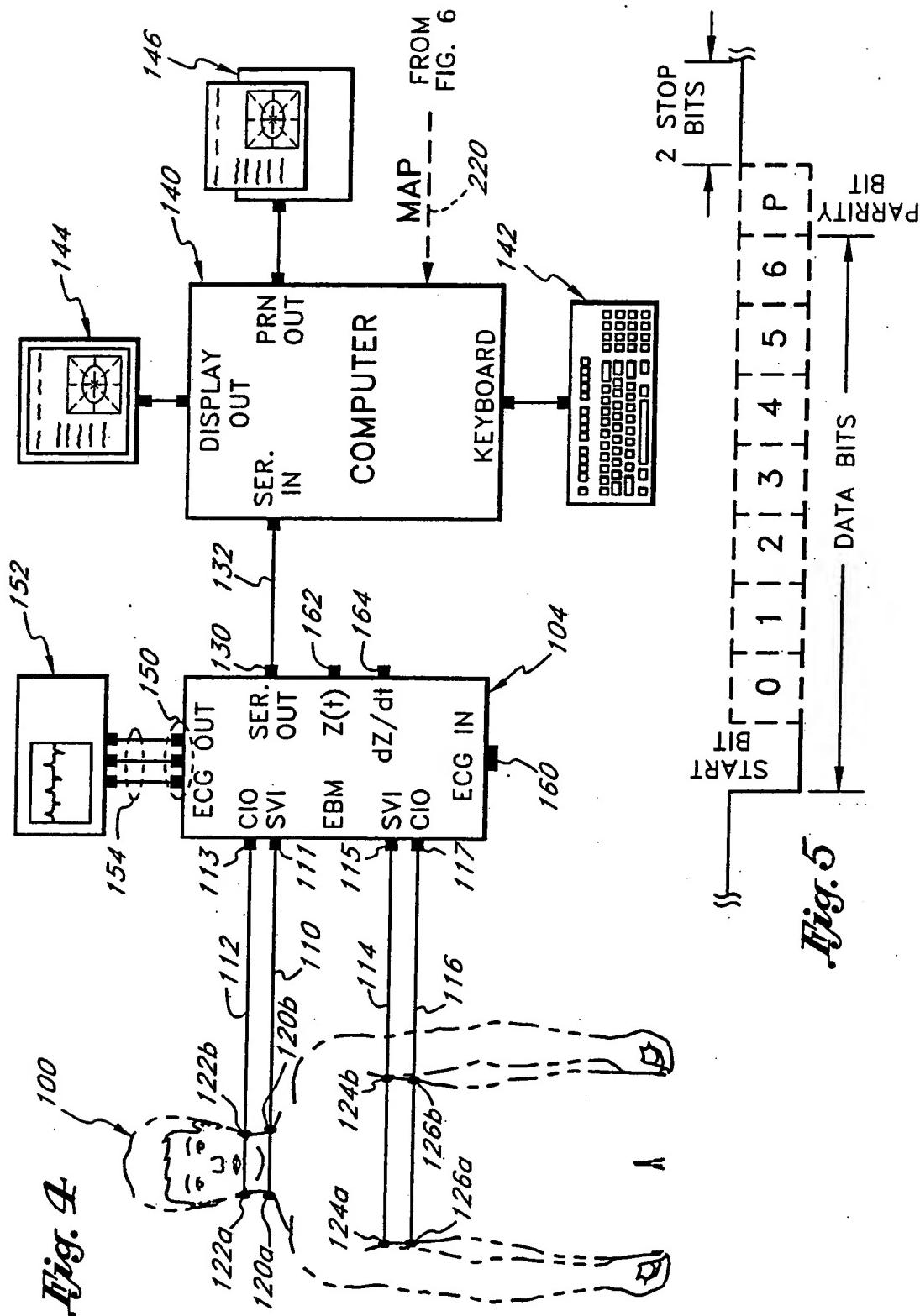
3.5

*Fig. 2*

3/11



4/11



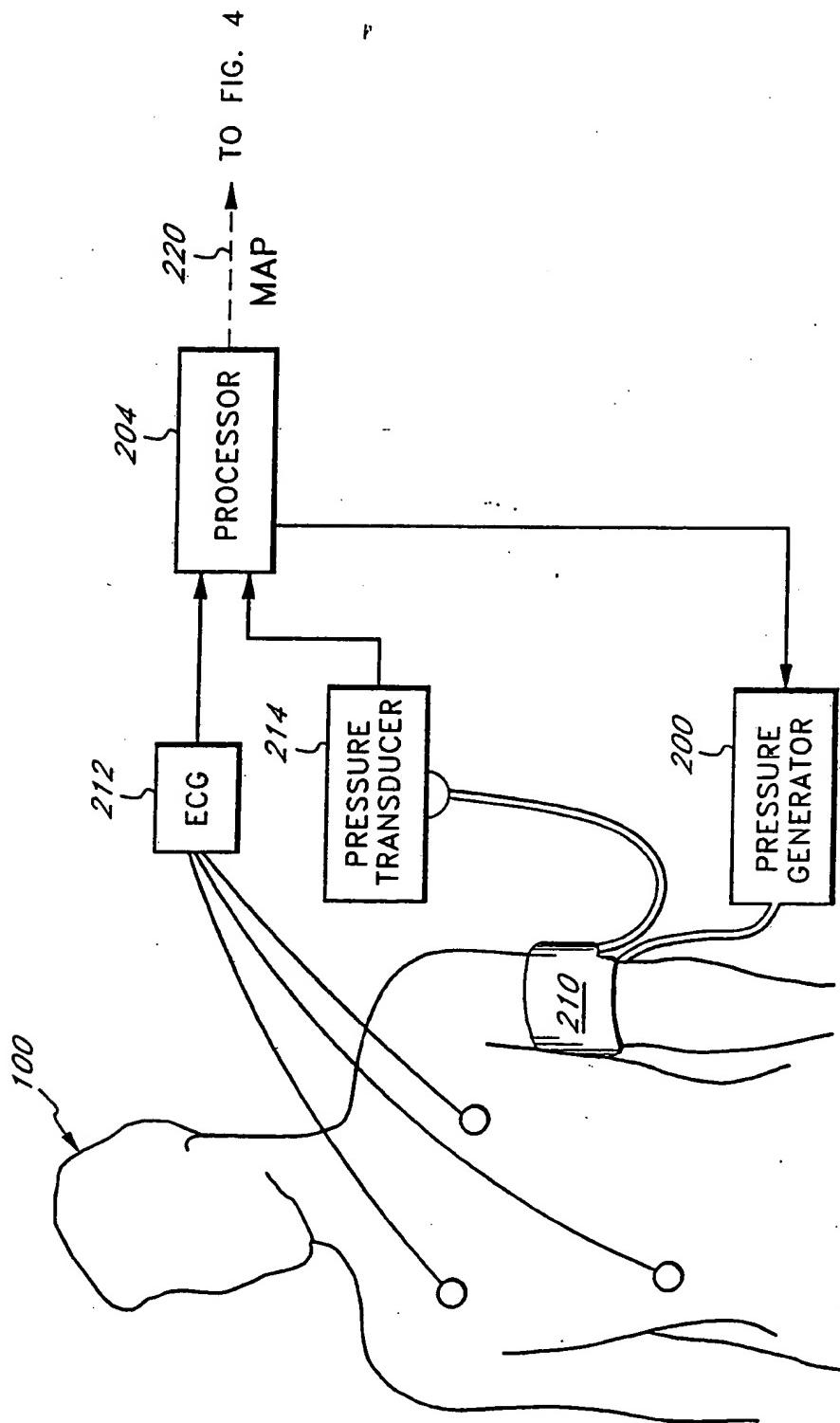
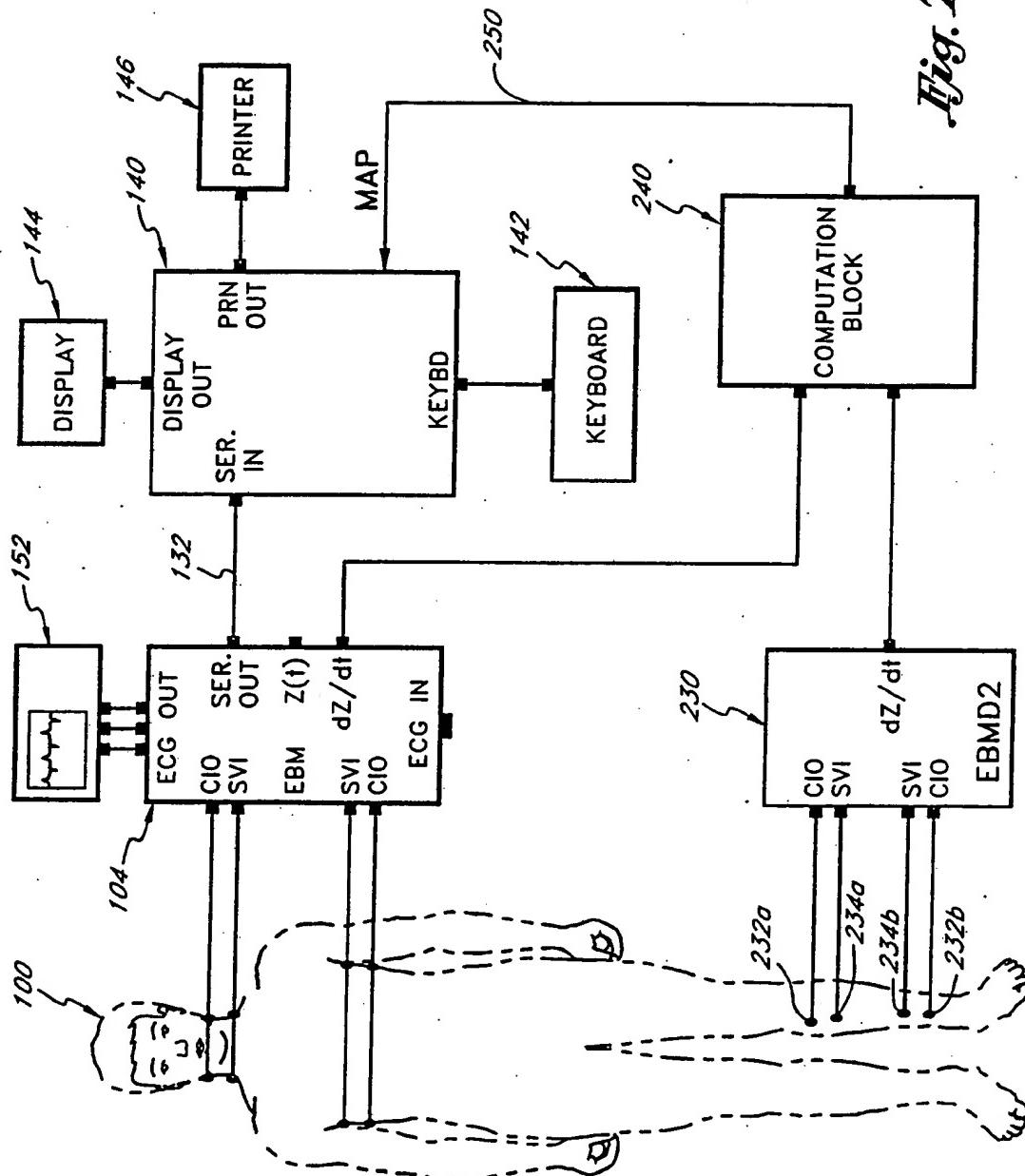


Fig. 6

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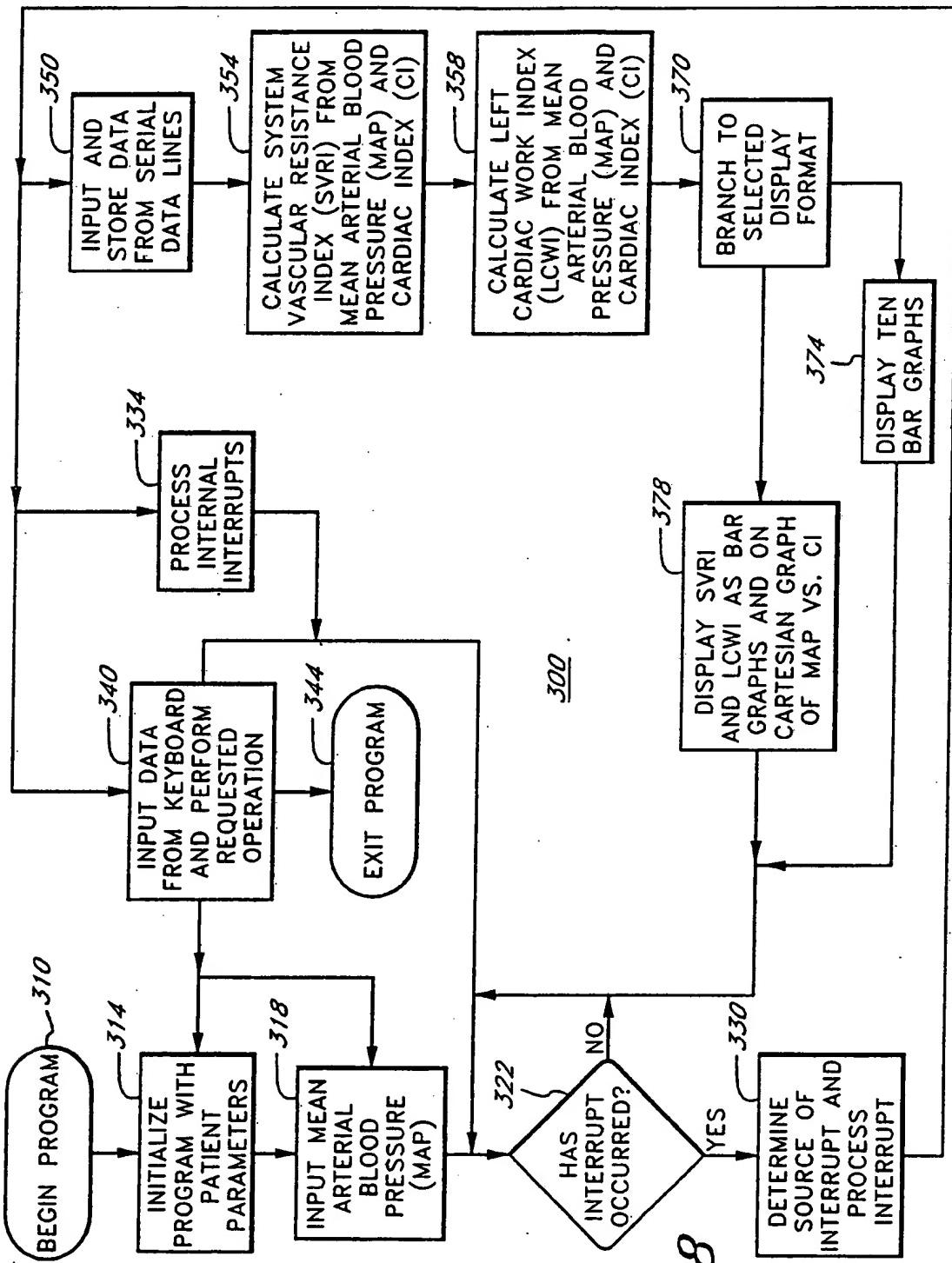


Fig. 8

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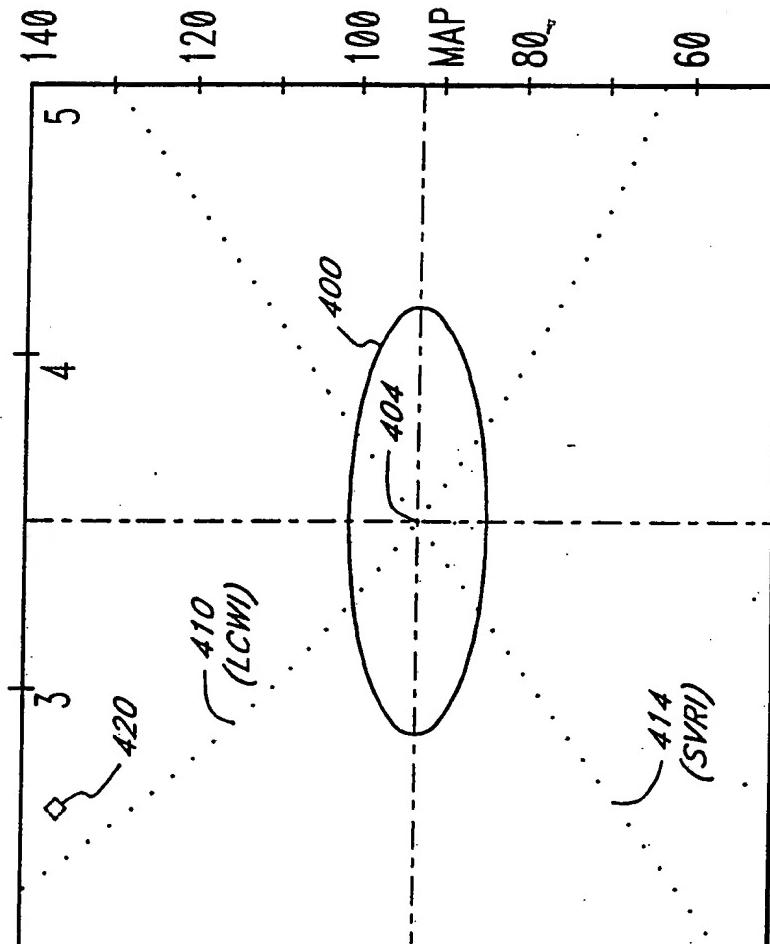
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HEMODYNAMIC / CARDIODYNAMIC DATA		©1988 BoMed
GLOBAL FLOW	Cf	2.8
PUMP PERFORMANCE	Si	30
PRELOAD	Eti	45
(volume)	Ic	.033
CONTRACTILITY (inotropy)	ACl	0.5
AFTERLOAD	SVRI	1660
CARDIAC WORK	LCWI	3.3
PUMP EFFICIENCY	EF	35
THORACIC FLUIDS	TFC	.030
MEAN ARTER.PRESS	MAP	84
382		HR = 60 beats/min
380		2.7 L/min/m ²
382		46 mL/m ²
380		96 mL/m ²
382		0.032/sec
380		0.89/sec ²
380		3870 F.0hm/m ²
380		5.0 kgm/m ²
380		65
380		47 %
380		0.033/0hm
380		135 Torr
380		Hg. 9

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.DOE JOHN , male, 03 15 25 ,175cm ,123kg

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HEMODYNAMIC STATUS

CI = 2.7 litres/min/m²
 MAP = 135 Torr
 LCWI = 5.0 kgm/m²
 SVRI = 3670 (F.0hm/m²)
 HR = 60 beats/min

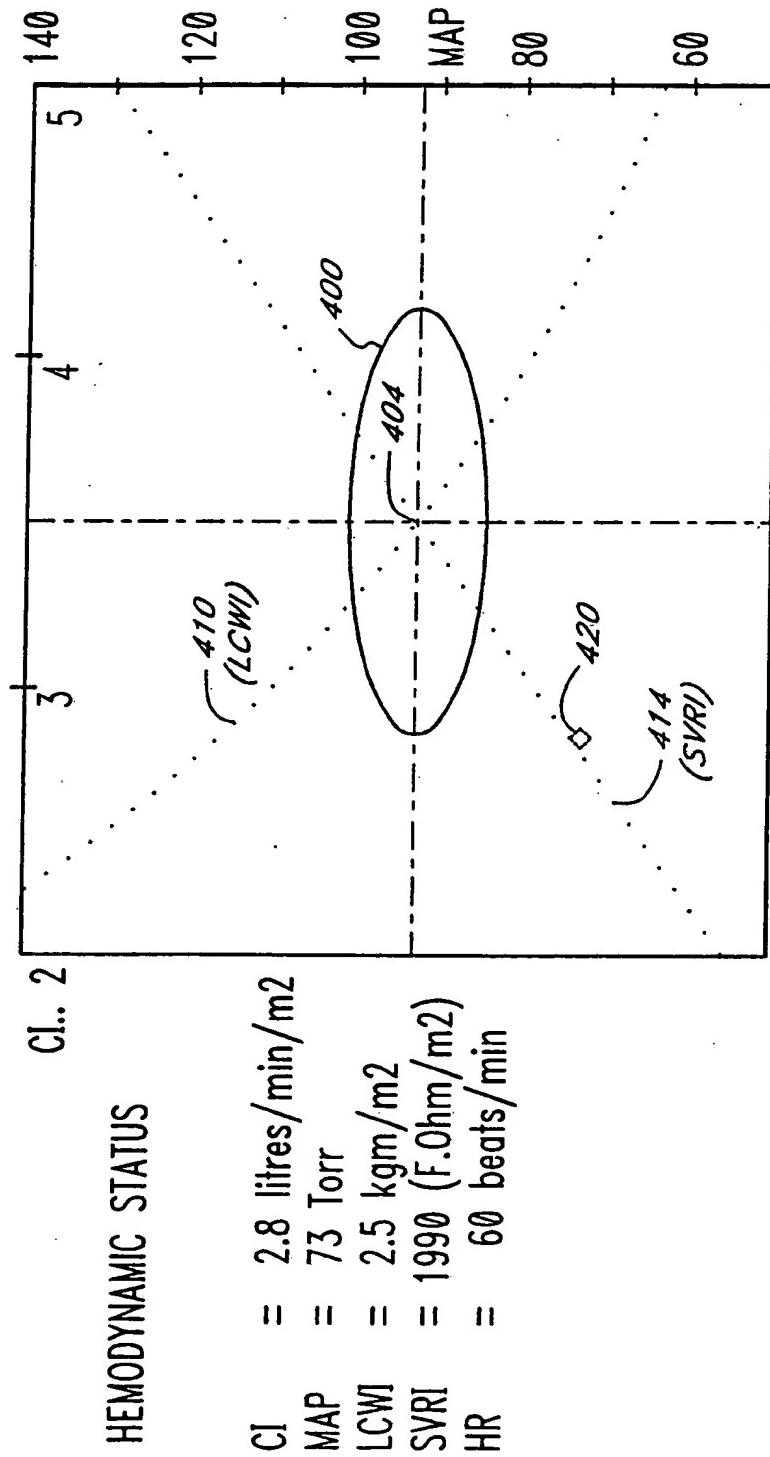
SUBSTITUTE SHEET

15 % relative hypervolemia and/or hyperinotropy.
 91 % relative arterial hypo-capacitance.

Fig. 10

DOE JANE , female ,12 31 27 ,160cm ,137kg

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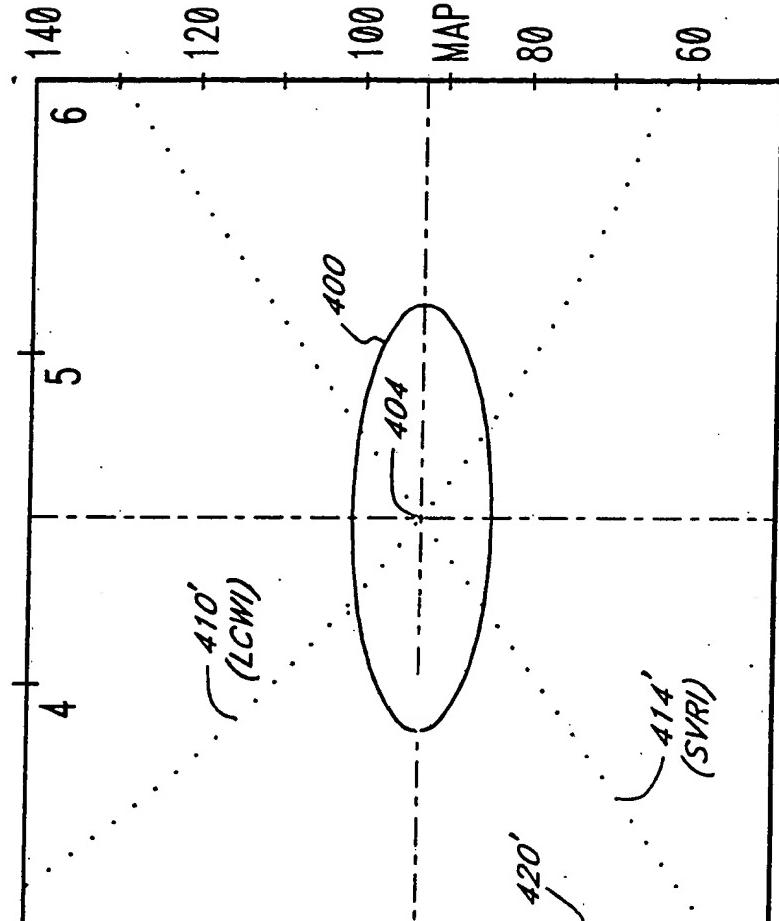
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Fig. II 43 % relative hypo-volemia and/or hypo-inotropy.
Arterial normocapacitance.

DOE JANE

, female ,12 31 27 ,160cm ,137kg

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HEMODYNAMIC STATUS

CI = 2.8 litres/min/m²
MAP = 73 Torr
LCWV = 2.5 kgm/m²
SVRI = 1990 (F.0hm/m²)
HR = 60 beats/min

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55 % relative hypo-volemia and/or hypo-inotropy.
26 % relative arterial hypo-capacitance.

Fig. 12

INTERNATIONAL SEARCH REPORT

International Application No. PCT/US89/03009

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) *

According to International Patent Classification (IPC) or to both National Classification and IPC

US CL. 128/693, 713, 734

INT CL(4) A61B 5/05

II. FIELDS SEARCHED

Minimum Documentation Searched ?

Classification System	Classification Symbols
US	128,693, 713, 734 600/16, 17

Documentation Searched other than Minimum Documentation
to the Extent that such Documents are Included in the Fields Searched §

III. DOCUMENTS CONSIDERED TO BE RELEVANT §

Category *	Citation of Document, ** with indication, where appropriate, of the relevant passages †‡	Relevant to Claim No. †§
Y	SRAMEK, "WHY SHOULD CARDIAC OUTPUT BE MEASURED/MONITORED," Consumer Information Bulletin, BoMed Medical Manufacturing, LTD., Irvine, California, March 1986. (See entire document).	1-22
Y	SHOEMAKER ET AL, "THERAPY OF CRITICALLY ILL POSTOPERATIVE PATIENTS BASED ON OUTCOME PREDICTION AND PROSPECTIVE CLINICAL TRIALS," Dept. of Surgery, Los Angeles County Harbor/UCLA Medical Center Torrance, California, August 1984. (See entire document).	1-22
A,P	US,A, 4,807,638 (SRAMEK), 28 February 1989. (See Figure 1).	1-22
A	US,E, RE. 30,101, (KUBICEK ET AL), 25 September 1979.	1-22
A	US,A, 4,437,469 (DJORDJEVICH ET AL), 20 March 1984.	1-22
A	US,A, 4,450,527 (SRAMEK), 22 May 1984.	1-22
A	US,A, 4,429,701 (GOOR ET AL), 07 February 1984.	1-22

* Special categories of cited documents: †
 "A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"A" document member of the same patent family

IV. CERTIFICATION

Date of the Actual Completion of the International Search

08 September 1989

Date of Mailing of this International Search Report

07 NOV 1989

International Searching Authority

RO/US

Signature of Authorized Officer

John C. Hanley